

Catastrophic Landslide of Hsiaolin Village Kinetic Process and Deposit through Geomorphologic Analysis and Numerical Simulation

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Abstract

On August 2009, Typhoon Morakot with torrential rainfall brought a catastrophic landslide which buried about 5 hundred people and village in Hsiaolin village, Jiasian Township, Kaohsiung County. Therefore, many studies investigated and estimated the landslide mechanism of Hsiaolin village. However, there were few research evidences to support a causal relationship between kinetic process and the hazard zonation. This research aims at the estimation of catastrophic landslide kinetic process and deposit in Hsiaolin village. Based on geomorphologic analysis and field investigation, the source area (Xiandu Mountain) of slide locates at a stream head was covered by very thick colluvium of different ages. Then, the source area is too height above the village and deposition area, which caused high dynamic energy and enlarged the impact of the landslide. Numerical modelling of Hsiaolin village is carried out using a 3D discrete element program, PFC3D (Itasca, 1999). The landslide from debris slide converted to debris avalanche during the kinetic process. When the friction coefficient of each particle is equal 0.05, the predicated maximum velocity is about 80m/sec and the debris could reach to the other side of the Chishan River. Consequently was resulted the dammed lake and buried most of Hsiaolin village.

Keywords: *Catastrophic landslide, Hsiaolin village, geomorphologic analysis, Numerical modelling*

Kinematics Process of Shiaolin Catastrophic Landslide through Geomorphologic Analysis and Numerical Simulation

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1

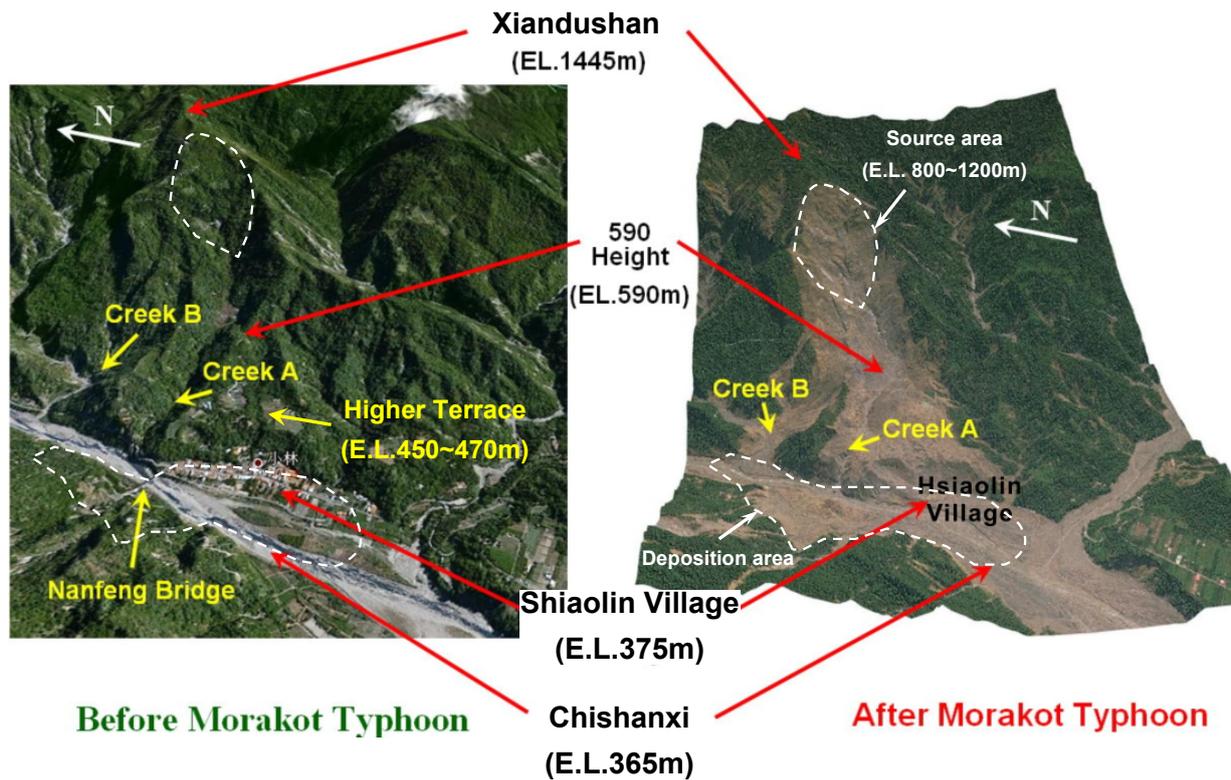
Outline

- Introduction
- Geomorphologic analysis
- Numerical Simulation
- Conclusion



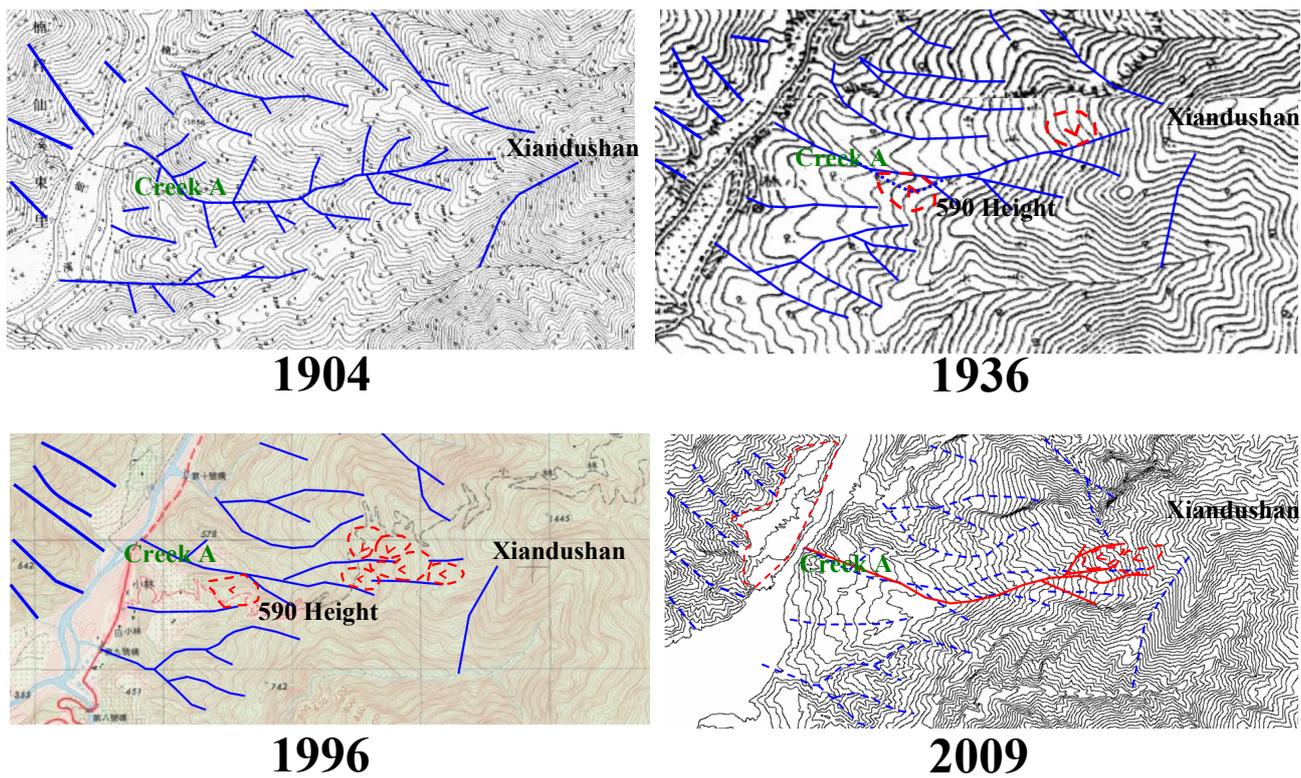
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Introduction- Topography of Shiaolin landslide



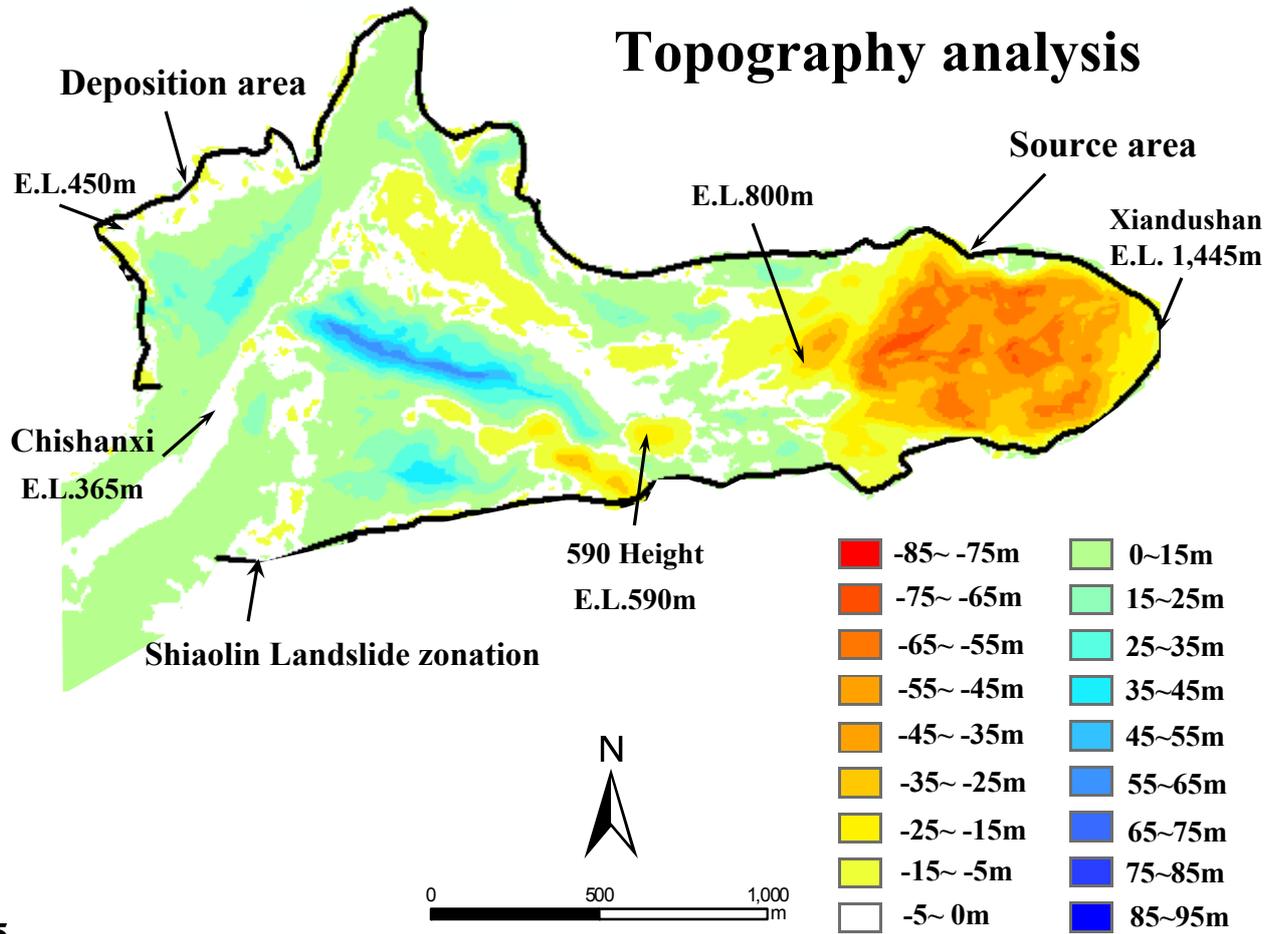
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Geomorphologic analysis



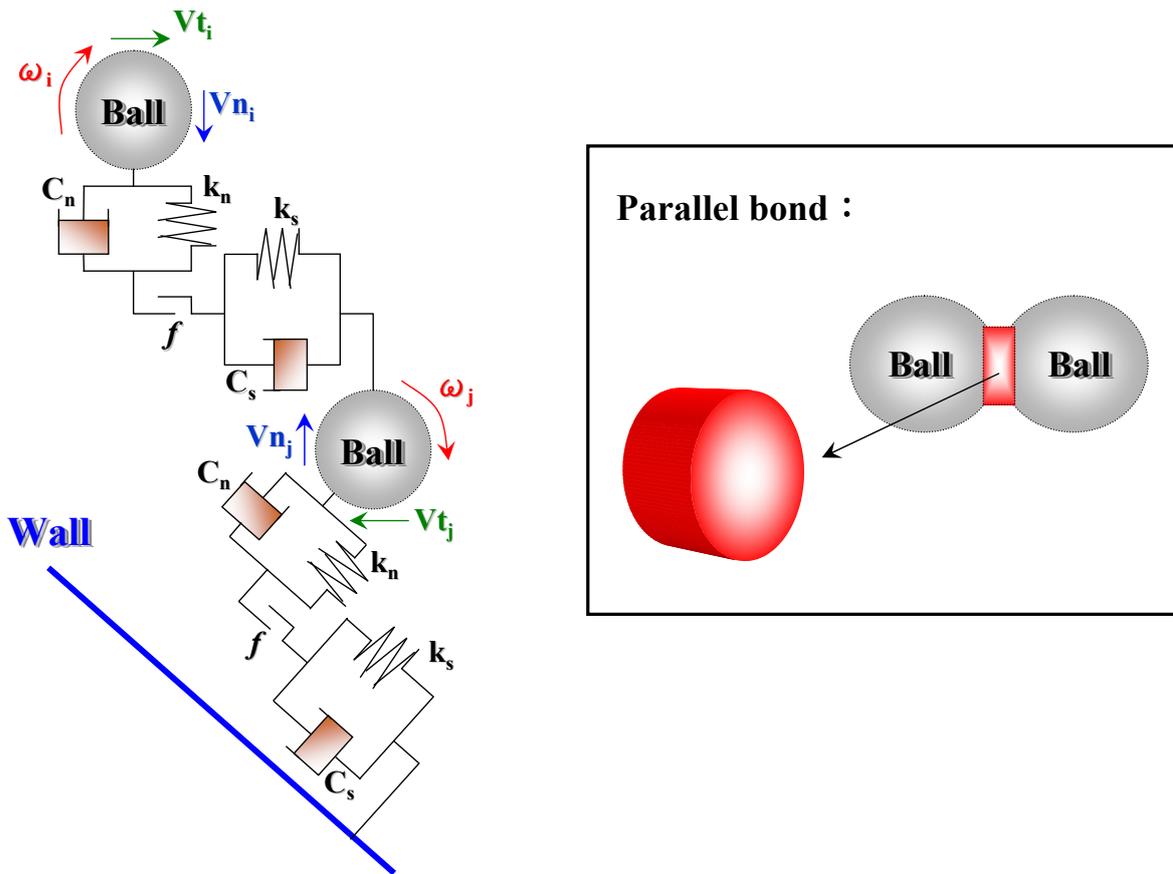
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Topography analysis



5

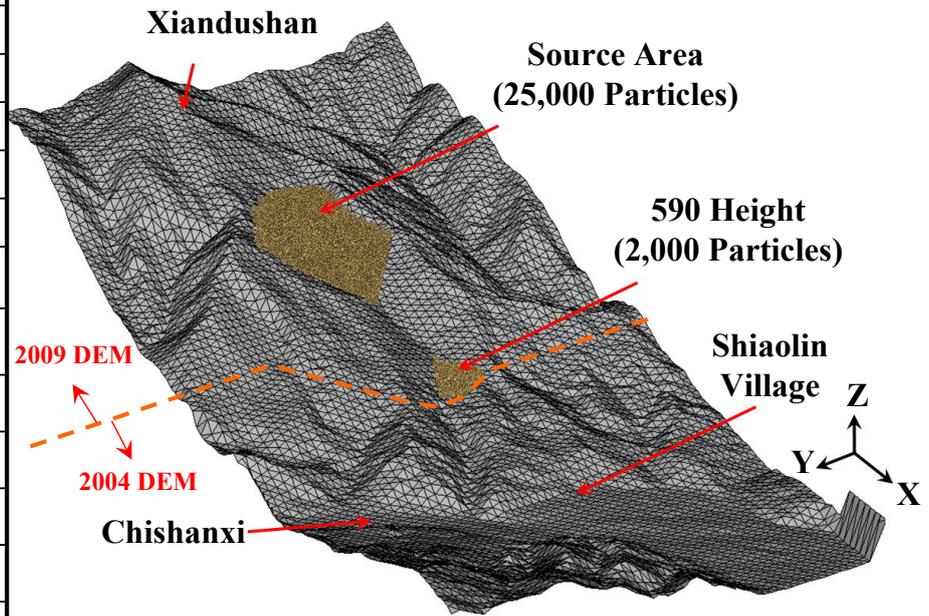
PFC Theory (Discrete Element Method)



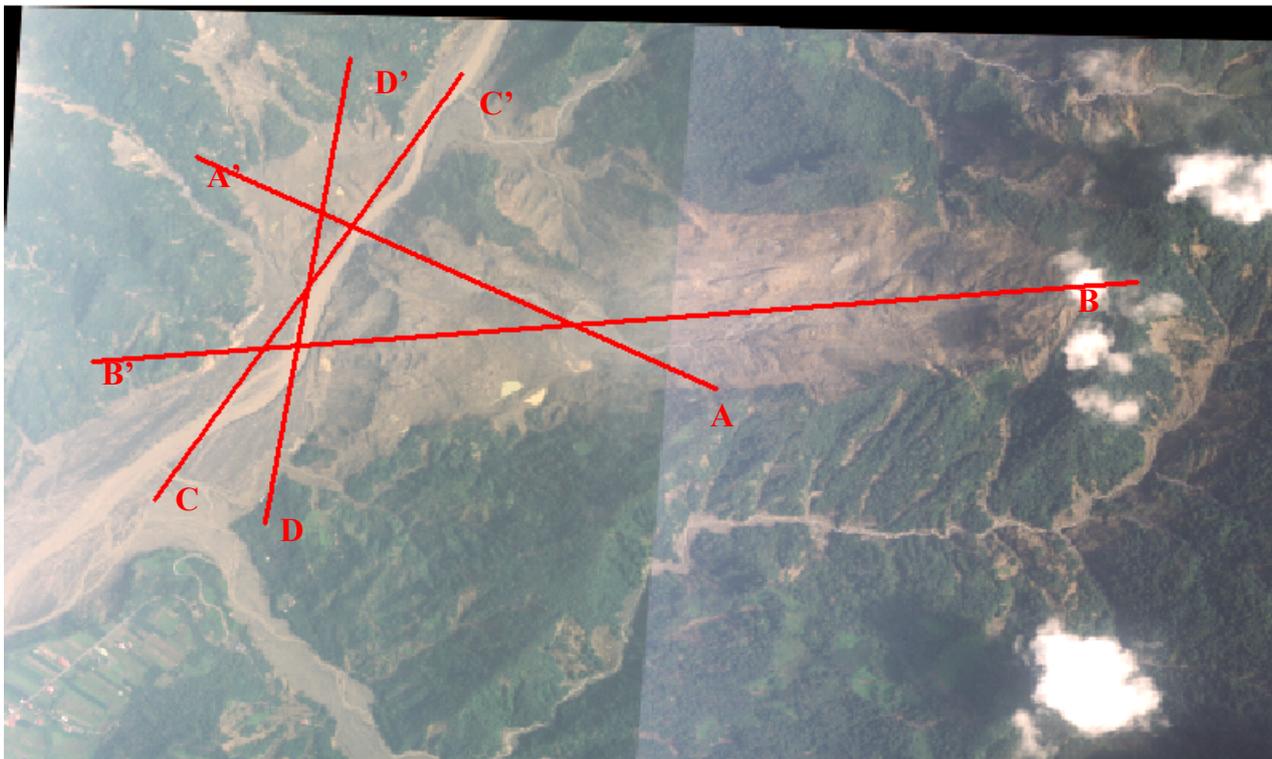
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Numerical modeling of Shiaolin landslide

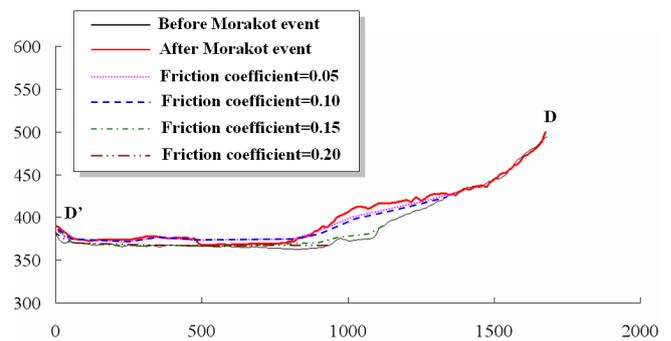
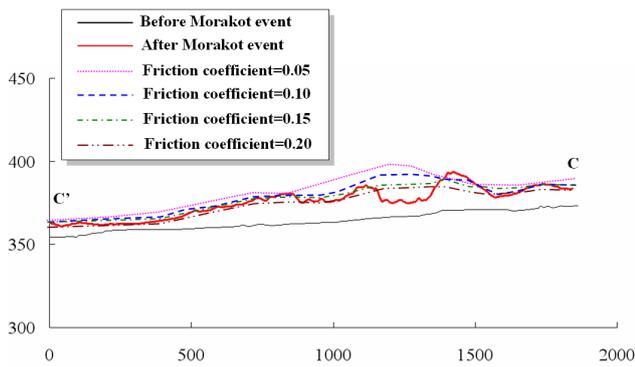
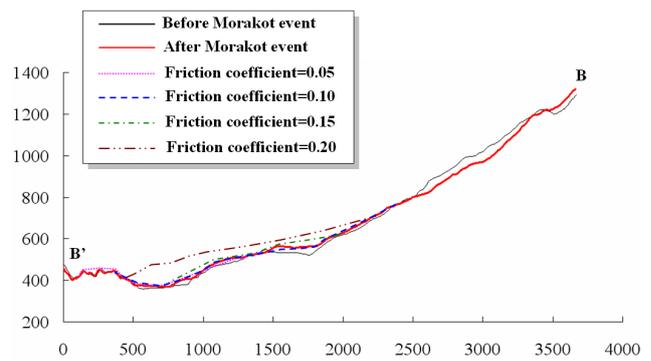
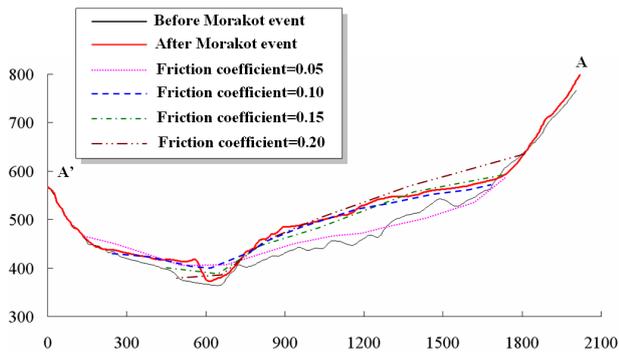
Landslide Volume (m ³)	2.3e8
Number of wall elements	13,456
Number of particles	27,000
Particle density (kg/cm ³)	2,600
Range of particle radius (m)	4-6
Normal stiffness (KN/m)	2e8
Shear stiffness (KN/m)	2e8
Friction coefficient of slip surface for each particle	0.05-0.2
Friction coefficient of wall	0.6
Normal stiffness of parallel bonds (KN/m ²)	2e8
Shear stiffness of parallel bonds (KN/m ²)	2e8
Normal strength of parallel bonds (KN/m ²)	2e6
Shear strength of parallel bonds (KN/m ²)	2e6
Critical damping ratio (Normal direction)	0.4
Critical damping ratio (Shear direction)	0.2



7



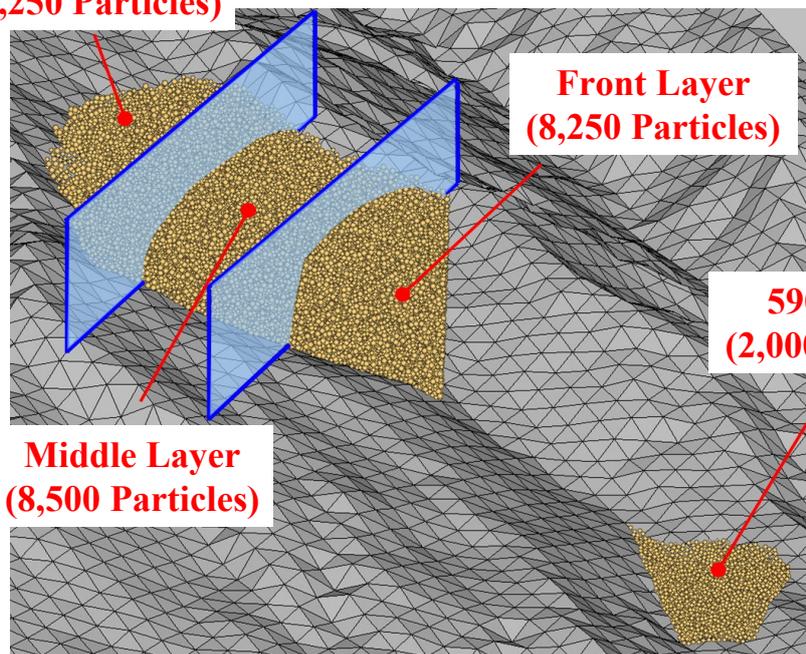
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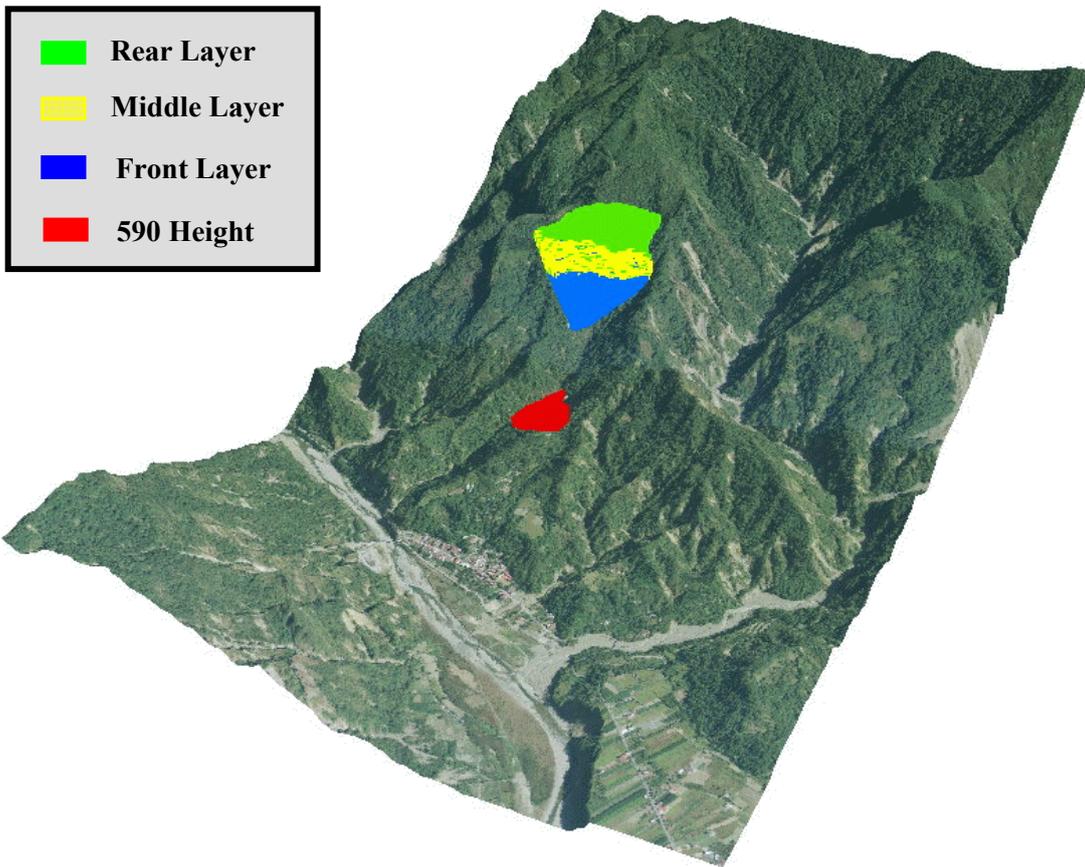


9

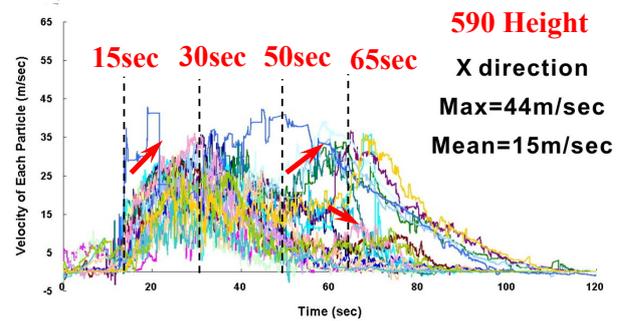
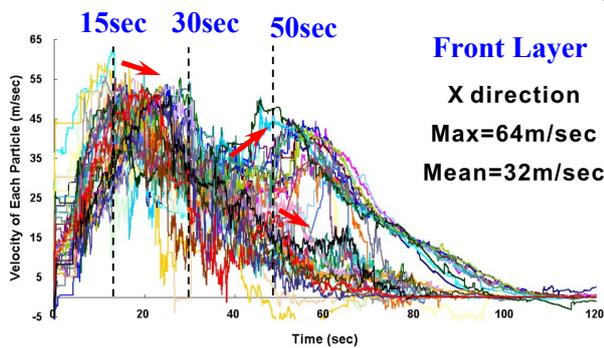
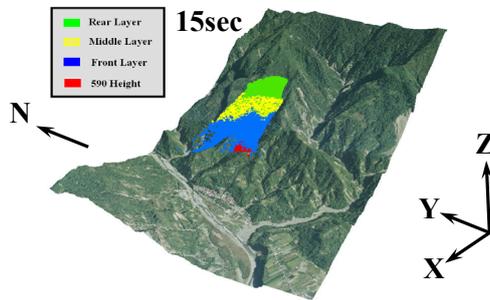
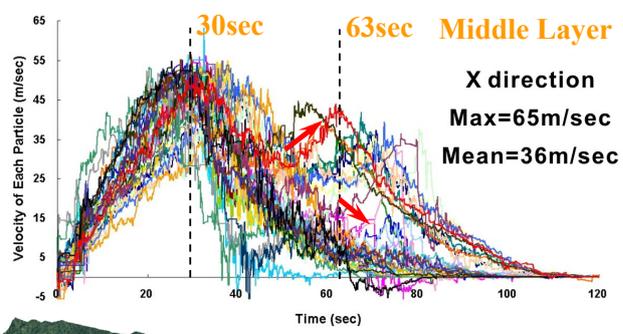
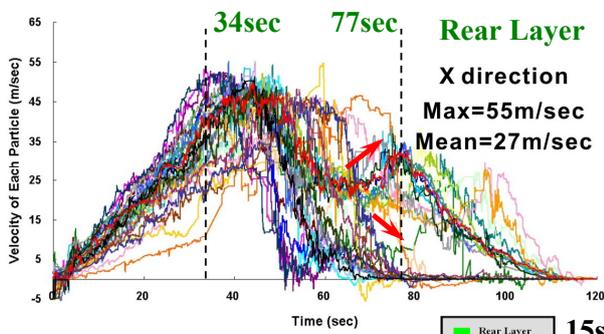
Numerical modeling of Shiaolin landslide

**Rear Layer
(8,250 Particles)**

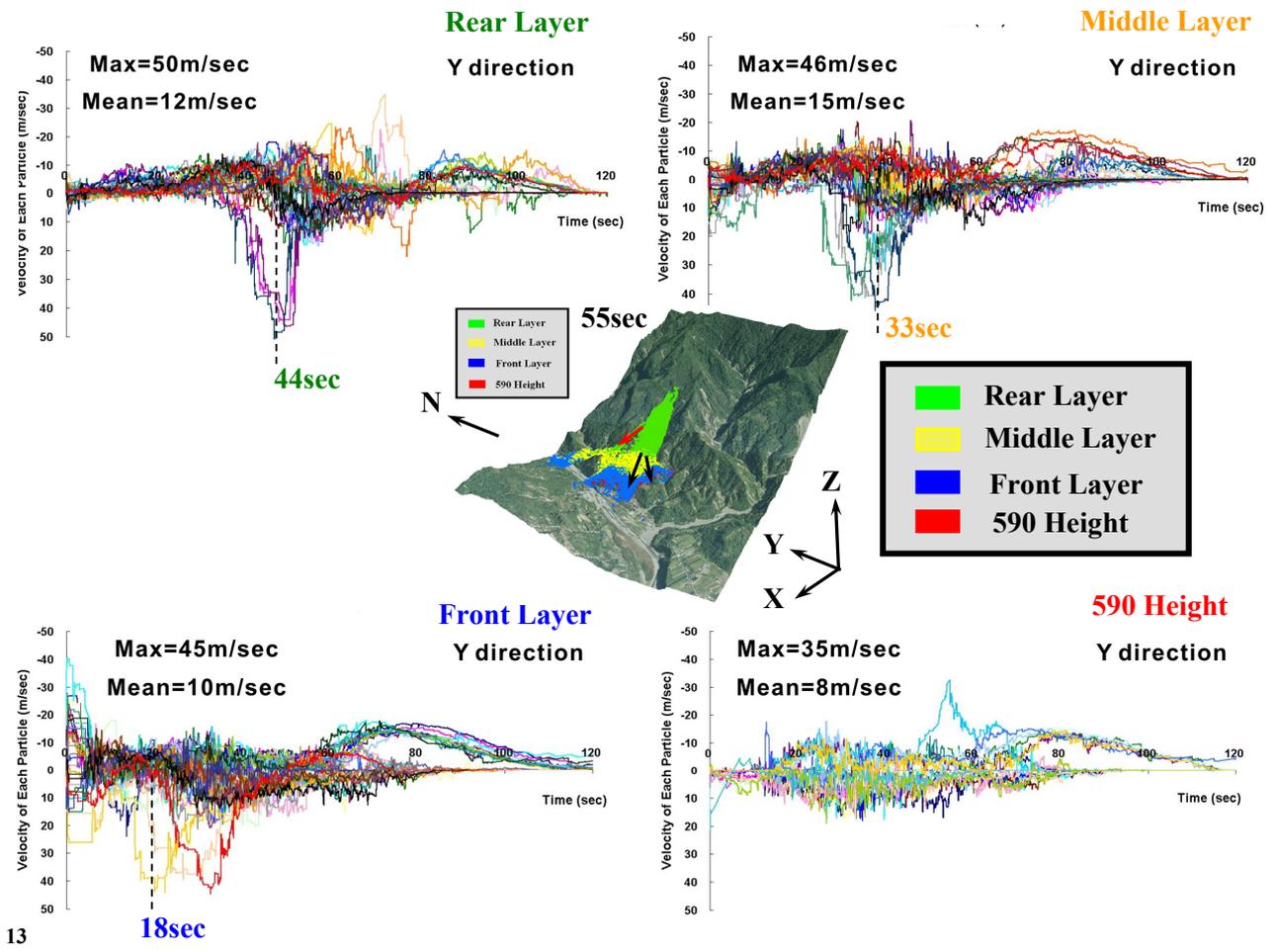




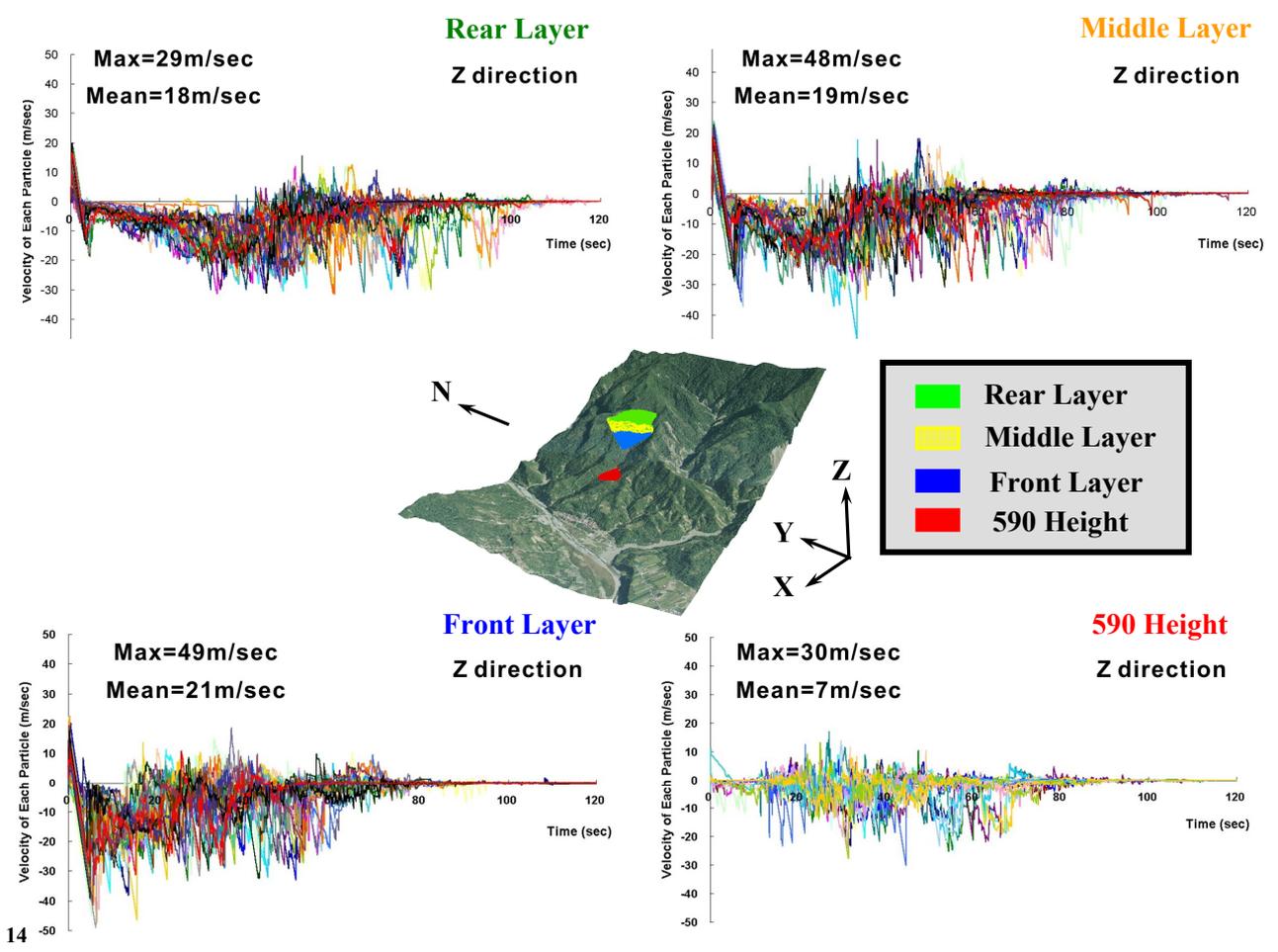
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12



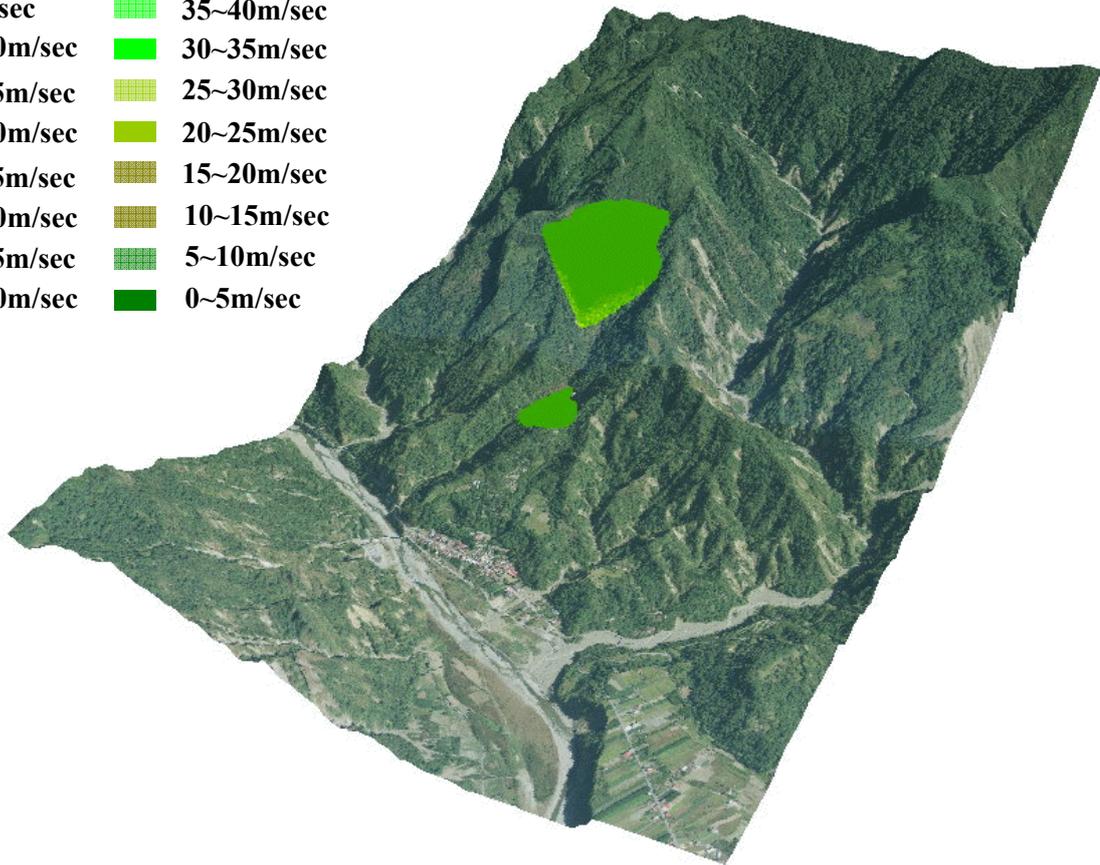
13



14

Velocity

 >80m/sec	 35~40m/sec
 75~80m/sec	 30~35m/sec
 70~75m/sec	 25~30m/sec
 65~70m/sec	 20~25m/sec
 60~65m/sec	 15~20m/sec
 55~60m/sec	 10~15m/sec
 50~55m/sec	 5~10m/sec
 45~50m/sec	 0~5m/sec



15

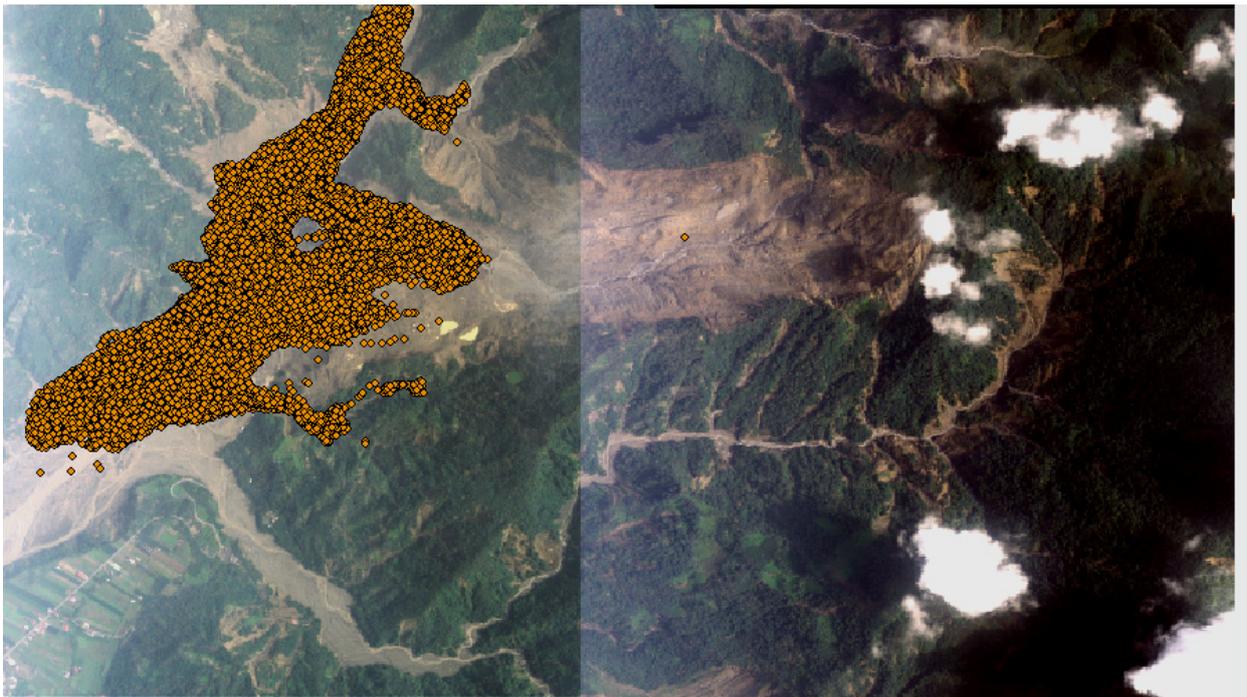
Conclusion

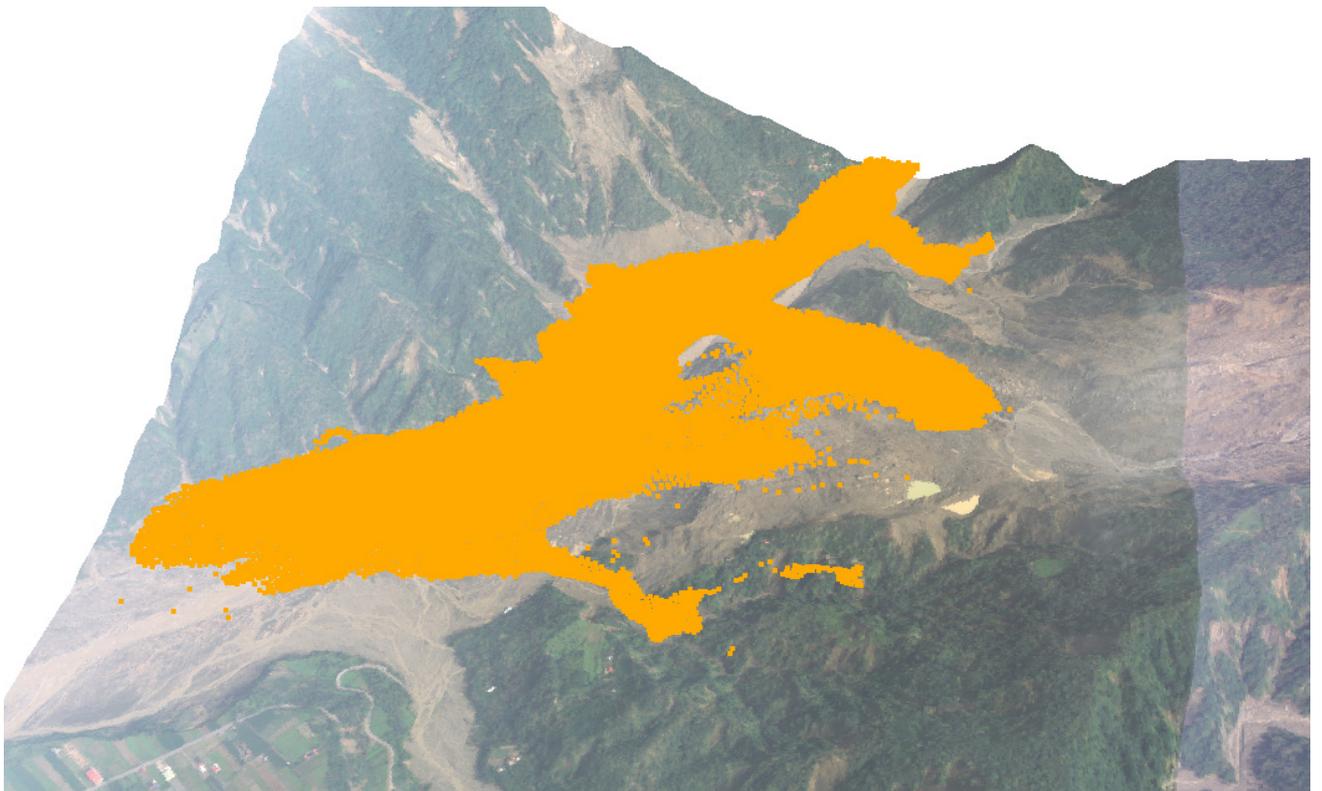
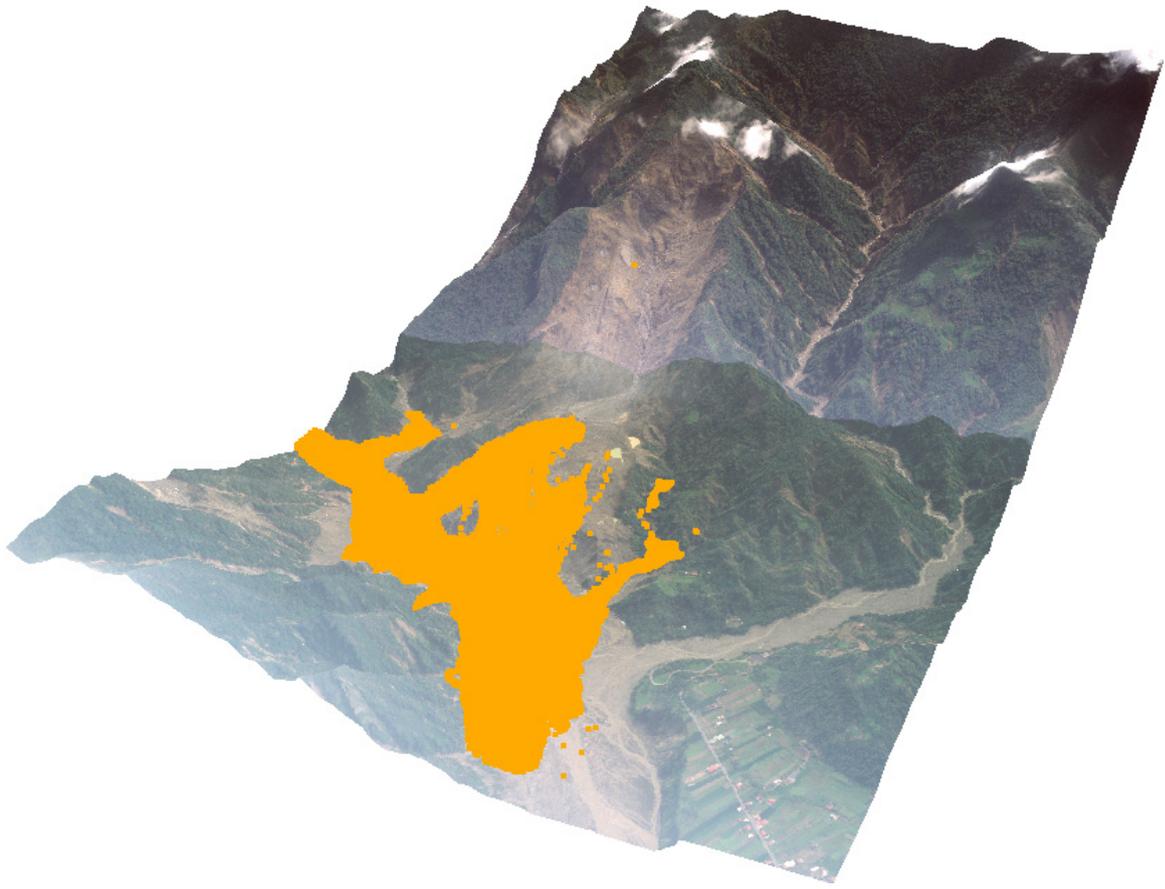
- The source area and the top of higher terrace was covered by **colluvium of different ages form 1936~2009.**
- When Shiaolin landslide reached 590 Height from the source area, **the steep terrain and the gravity controlled the landslide motion.**
- When 590 Height collapsed for Shiaolin catastrophic landslide and caused the hummocky terrain transformed the smooth terrain, which **provide the debris avalanche overflow the higher terrace and buried Shiaolin village.**



16

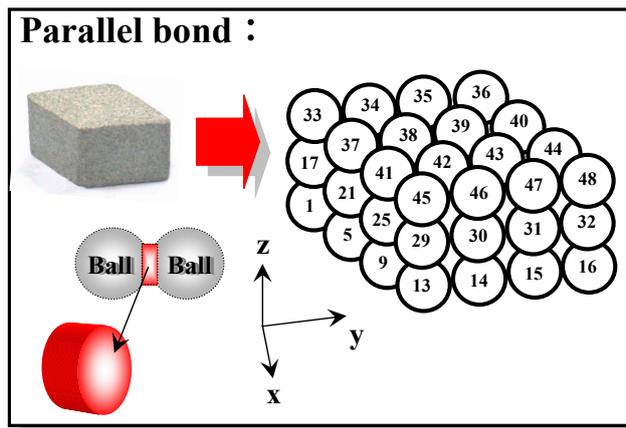
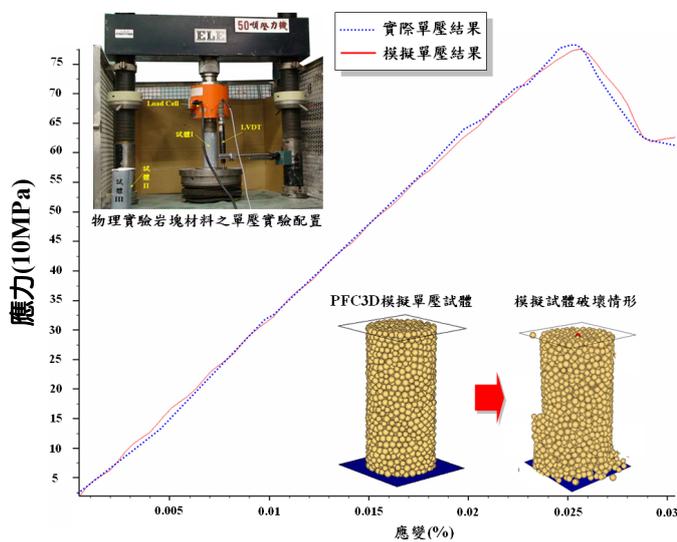
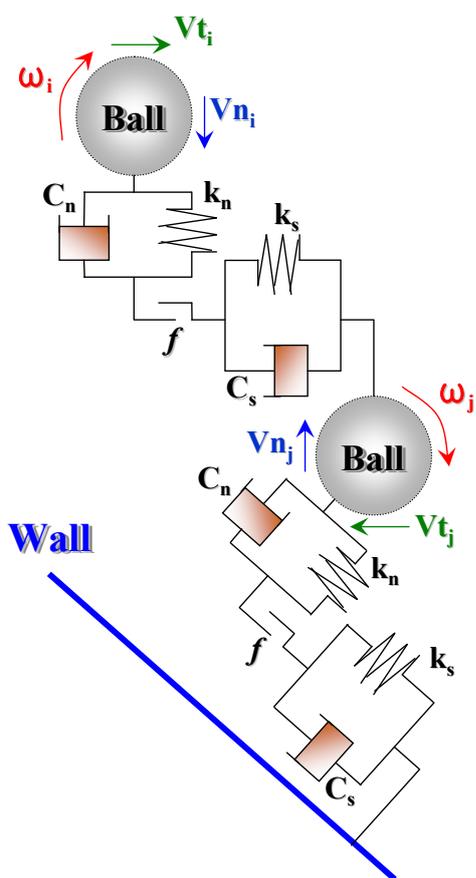
Thanks for Listening





Simulation parameters

PFC 3D 原理:



How to set the parameters?

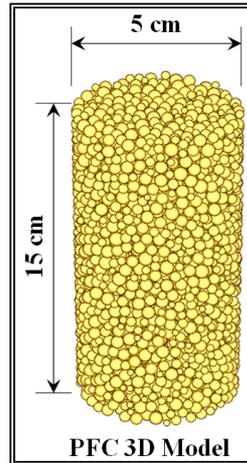
Material properties:

Density: 2500kg/m^3

Friction angle: 37°

Particle Size: $0.0005\sim 0.001\text{m}$

5555 Particles



試體單壓配置

Simulation Parameters:

Contact Bonds:

Normal Strength (N)

Shear Strength (N)

Parallel Bonds:

Parallel Bond Stiffness (N/m^3)

Parallel Bond Strength (N/m^3)

Normal Strength (N/m^2)

Shear Strength (N/m^2)

23

PFC (2002) and Potyondy (2004)

Particle Size: $0.0005\sim 0.001\text{m}$

$R=(0.0005+0.001)/2=0.00075$

$kn=4 \cdot R \cdot Ec=4.16 \cdot 10^7 \sim 1.12 \cdot 10^8 \text{N/m}$

$Kn/ks=1$

Contacts Bond:

$kn=4 \cdot R \cdot \sigma_c=2.5 \cdot 10^5 \sim 5.0 \cdot 10^5 \text{N}$

$Kn/ks=1$

Parallel Bond:

$L=0.0005+0.001=0.0015\text{m}$

$kn=Ec/L=20.8 \cdot 10^9/0.0015=1.4 \cdot 10^{13} \text{N/m}^3$

$Kn/ks=1$

$\sigma_c''=T/A+M \cdot R/I$ —先假設採用 $0.1 \sigma_c=12.5\text{MPa}$

$\tau_c''=V/A$ —先假設採用 $\sigma_c/2=6.25\text{MPa}$

Really Test: (Shi et al., 1994)

Peck Strength=125Mpa

Strain=0.6%

$E=20.8\text{GPa}$

PFC3D Test:

Peck Strength=1554Mpa

Strain=12.4%

$E=12.5\text{GPa}$

實際試驗與PFC3D測試結果

Step= $2.2 \cdot 10^5$

Particle Stiffness:

Normal Stiffness= $1 \cdot 10^8 \sim 2 \cdot 10^8 \text{N/m}$

Shear Stiffness= $1 \cdot 10^8 \sim 2 \cdot 10^8 \text{N/m}$

Contact Bond:

Normal Contact Bond= $2.2 \cdot 10^3 \sim 3.2 \cdot 10^3 \text{N}$

Shear Contact Bond= $2.2 \cdot 10^3 \sim 3.2 \cdot 10^3 \text{N}$

Parallel Bond:

Normal Stiffness= $1.4 \cdot 10^{13} \text{N/m}^3$

Shear Stiffness= $1.4 \cdot 10^{13} \text{N/m}^3$

Normal Strength= $1.25 \cdot 10^7 \text{N/m}^2$

Shear Strength= $6.25 \cdot 10^6 \text{N/m}^2$

Really Test: (Shi et al., 1994)

Peck Strength=125Mpa

Strain=0.6%

$E=20.8\text{GPa}$

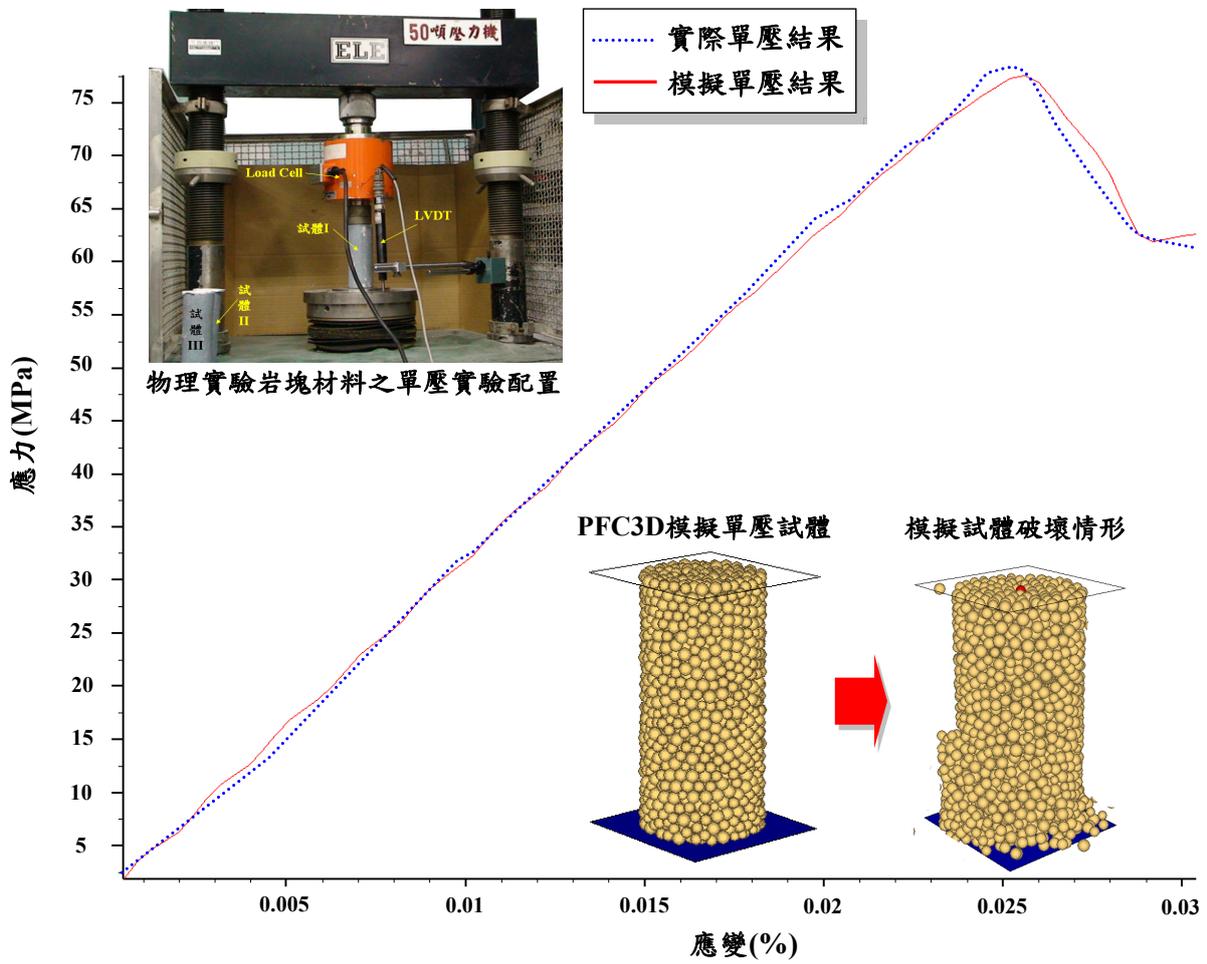
PFC3D Test:

Peck Strength=122Mpa

Strain=0.62%

$E=19.7\text{GPa}$

24



實際試驗與PFC3D測試結果

Step= 2.2×10^5

Particle Stiffness:

Normal Stiffness= $1 \times 10^8 \sim 2 \times 10^8 \text{N/m}$

Shear Stiffness= $1 \times 10^8 \sim 2 \times 10^8 \text{N/m}$

Normal Contact Bond= $2.2 \times 10^3 \sim 3.2 \times 10^3 \text{N}$

Shear Contact Bond= $2.2 \times 10^3 \sim 3.2 \times 10^3 \text{N}$

Parallel Bond:

Normal Stiffness= $1.4 \times 10^{13} \text{N/m}^3$

Shear Stiffness= $1.4 \times 10^{13} \text{N/m}^3$

Normal Strength= $1.25 \times 10^7 \text{N/m}^2$

Shear Strength= $6.25 \times 10^6 \text{N/m}^2$

Really Test: (Shi et al., 1994)

Peck Strength=125Mpa

Strain=0.6%

E=20.8GPa

PFC3D Test

Peck Strength=122Mpa

Strain=0.62%

E=19.7GPa

Test Simulation:

Particle Size: 0.0005~0.001m

Particle Stiffness:

$kn=10 \cdot R \cdot Ec$; $kn/ks=1$

Contacts Bond:

$kn=0.04 \cdot R \cdot \sigma_c$; $Kn/ks=1$

Parallel Bond:

$kn=Ec/L$; $kn/ks=1$

$\sigma_c''=T/A+M \cdot R/I$ —假設採用 $0.1 \sigma_c$

$\tau_c''=V/A$ —假設採用 $0.5 \sigma_c$

Case Study Simulation:

Particle Size: 0.5~1.0m

Particle Stiffness:

$kn=10 \cdot R \cdot Ec=1 \cdot 10^{11} \sim 2 \cdot 10^{11} \text{N/m}$

$Kn/ks=1$

Contact Bond:

$kn=0.04 \cdot R \cdot \sigma_c=2.5 \cdot 10^6 \sim 5 \cdot 10^6 \text{N}$

$Kn/ks=1$

Parallel Bond:

$L=0.5+1=1.5\text{m}$

$kn=Ec/L=1.4 \cdot 10^{10} \text{N/m}^3$

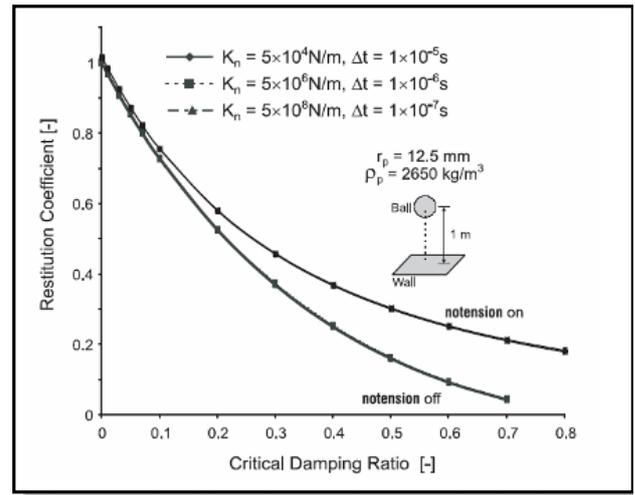
$Kn/ks=1$

$\sigma_c''=T/A+M \cdot R/I$ —假設採用 12.5MPa

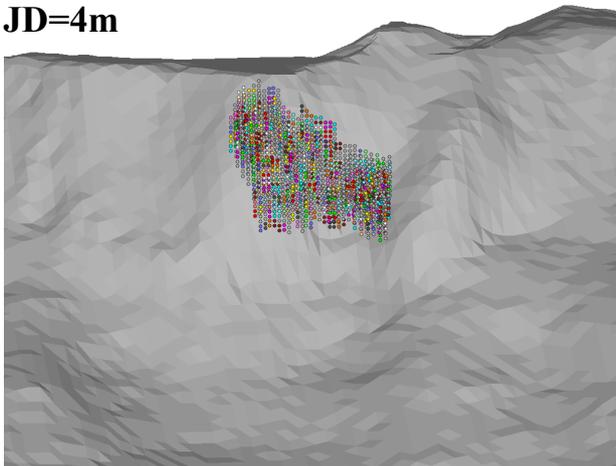
$\tau_c''=V/A$ —假設採用 6.25MPa

表 3.7 現地阻尼參數轉換一覽表(改自 Giani, 1992)

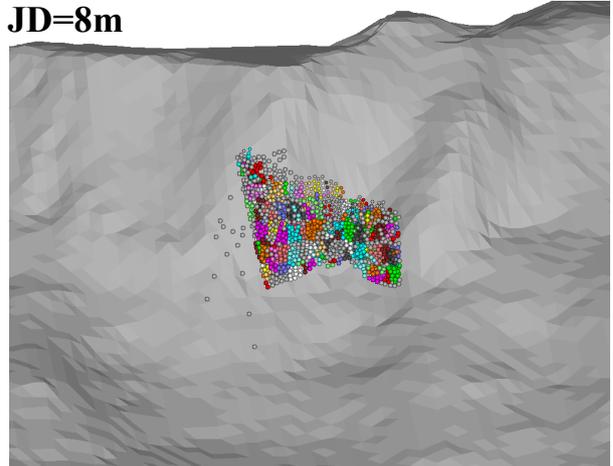
	正向回彈係數	轉換正向阻尼比	切向回彈係數	轉換切向阻尼比
Bedrock	0.50	0.21	0.95	0.02
Bedrock covered by large blocks	0.35	0.32	0.85	0.05
Debris formed by uniform distributed elements	0.30	0.36	0.70	0.11
Soil covered vegetation	0.25	0.40	0.55	0.20



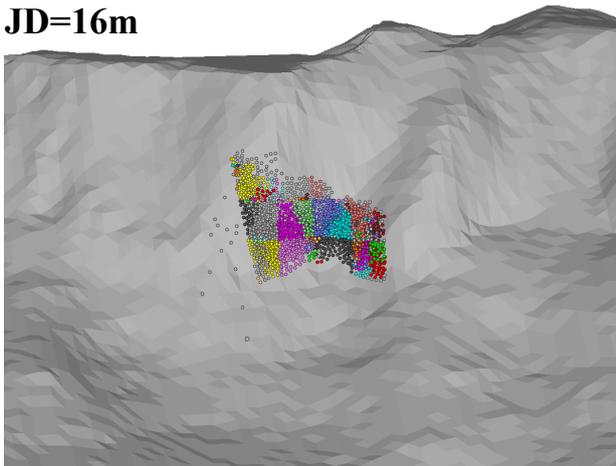
JD=4m



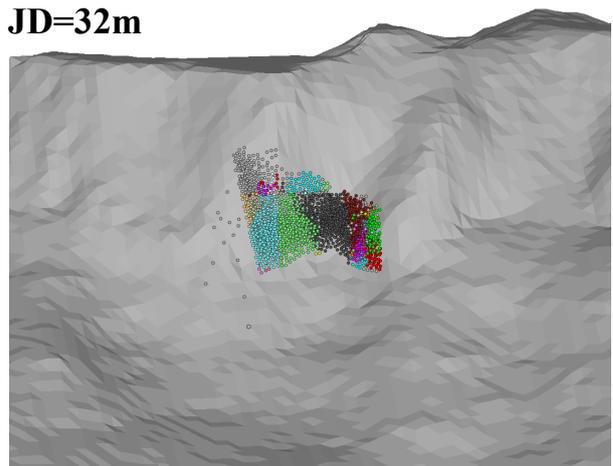
JD=8m



JD=16m



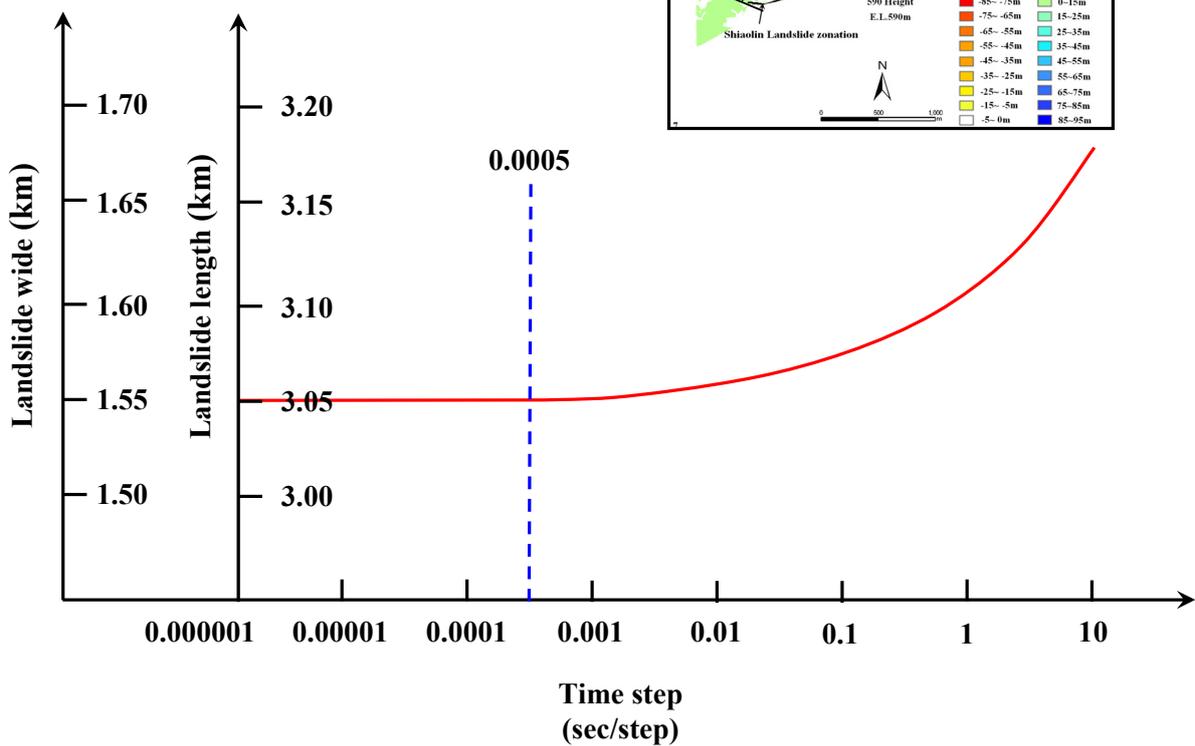
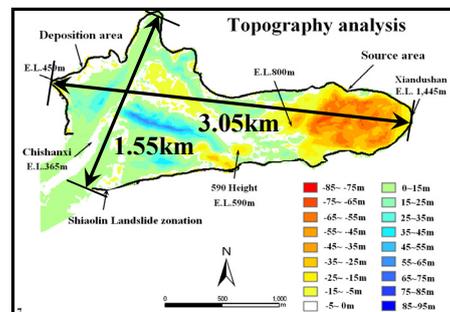
JD=32m



Simulation tests

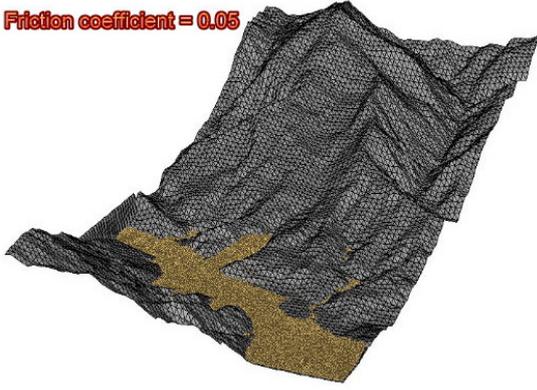
The length of landslide zonation = 3.05km

The wide of landslide zonation = 1.55km

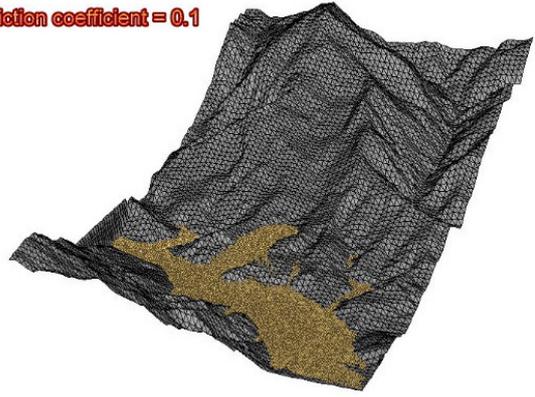


Influence of friction coefficient

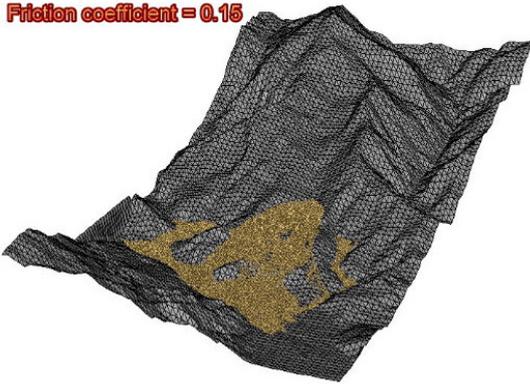
Friction coefficient = 0.05



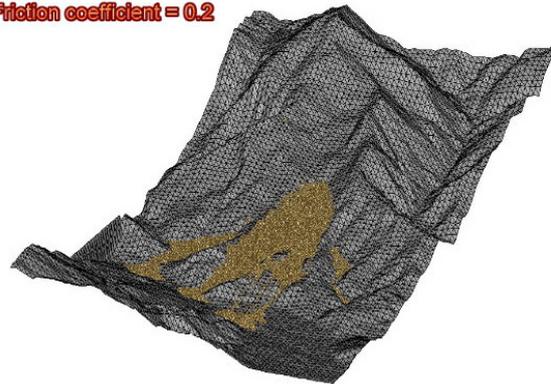
Friction coefficient = 0.1



Friction coefficient = 0.15



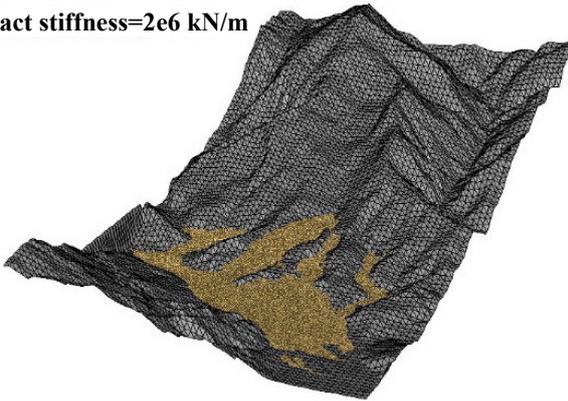
Friction coefficient = 0.2



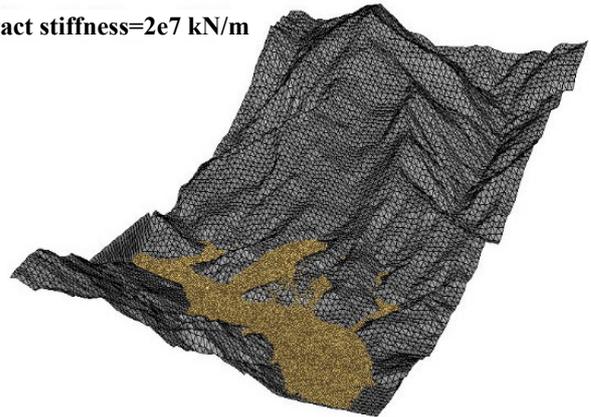
31

Influence of contact stiffness

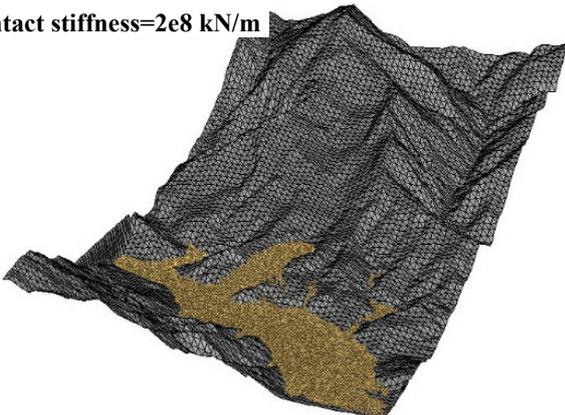
Contact stiffness=2e6 kN/m



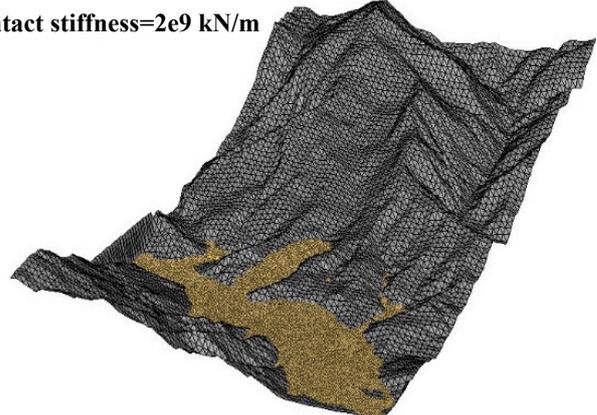
Contact stiffness=2e7 kN/m



Contact stiffness=2e8 kN/m

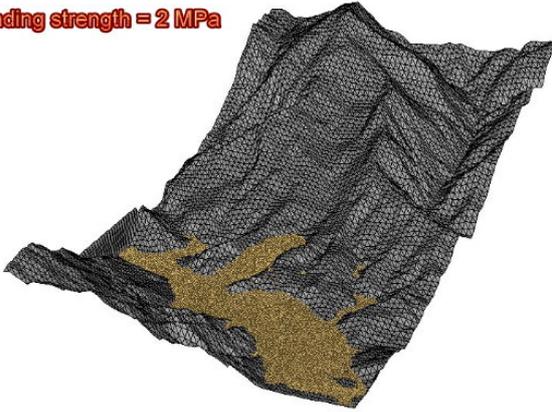


Contact stiffness=2e9 kN/m

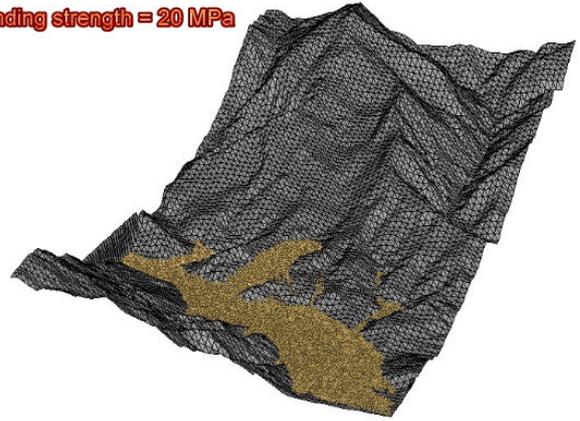


32

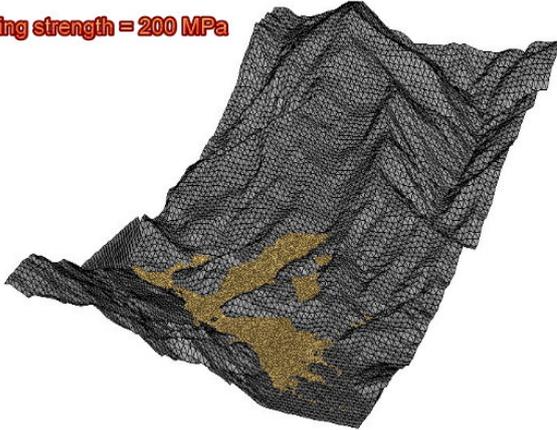
Bonding strength = 2 MPa



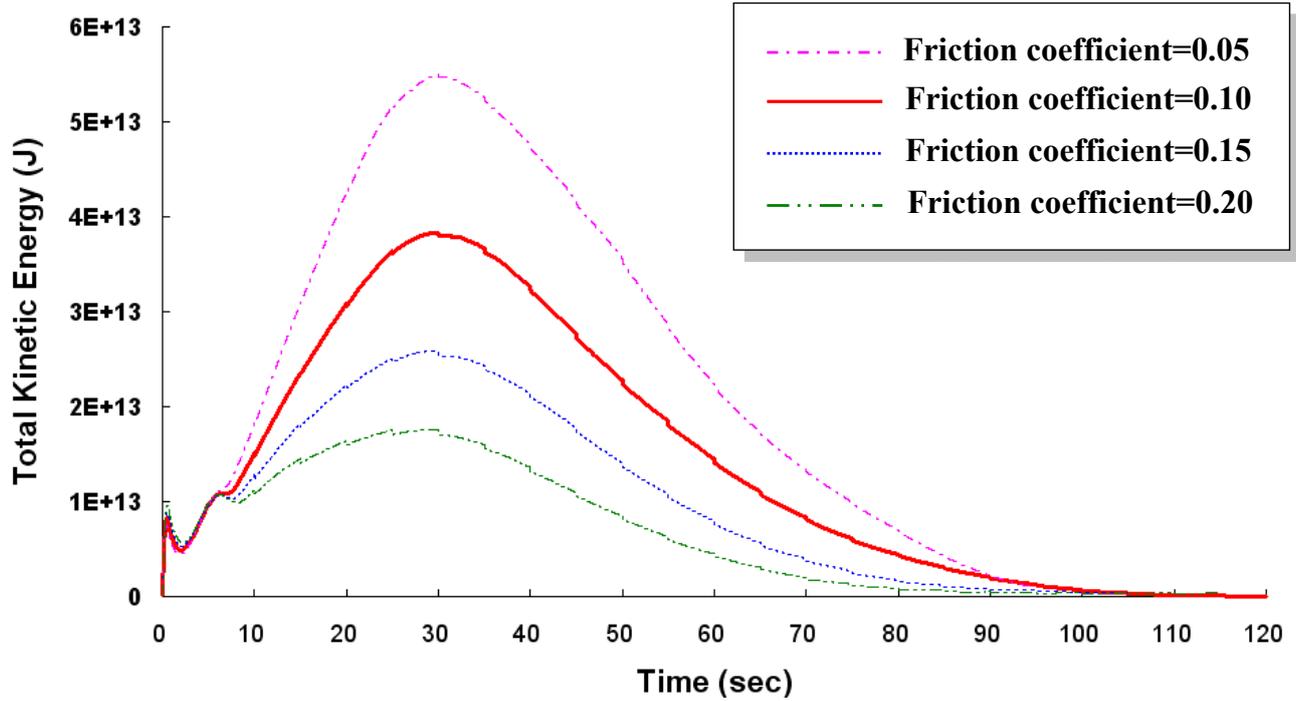
Bonding strength = 20 MPa



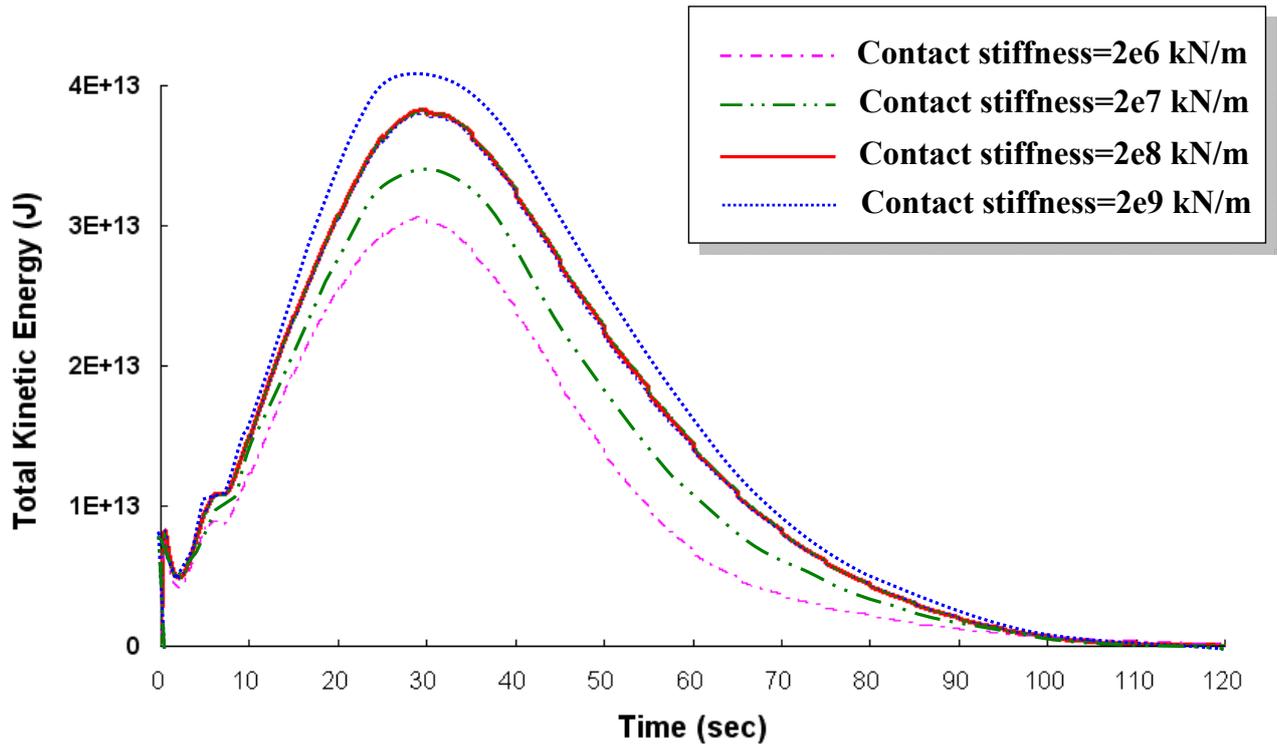
Bonding strength = 200 MPa



33

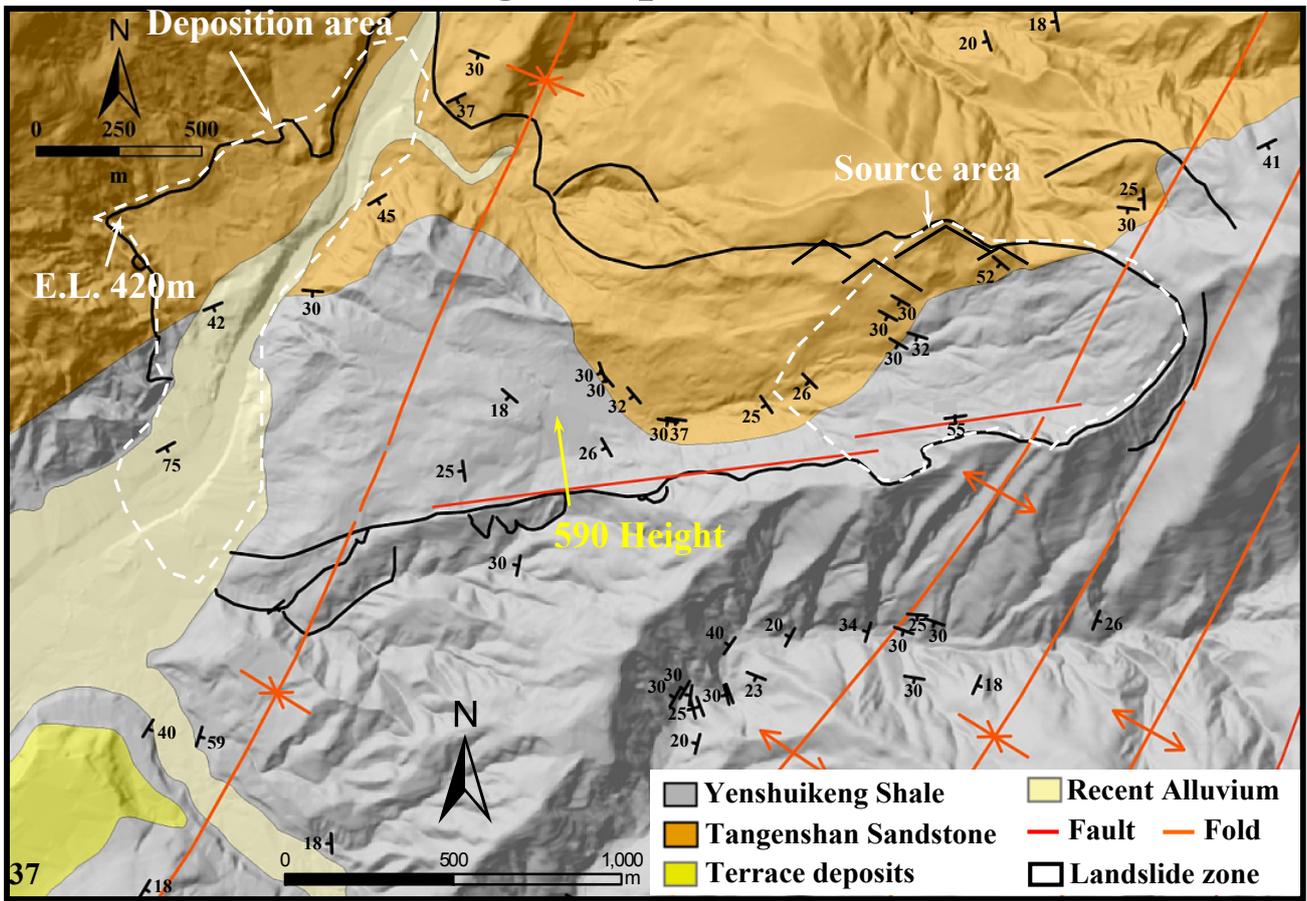


34

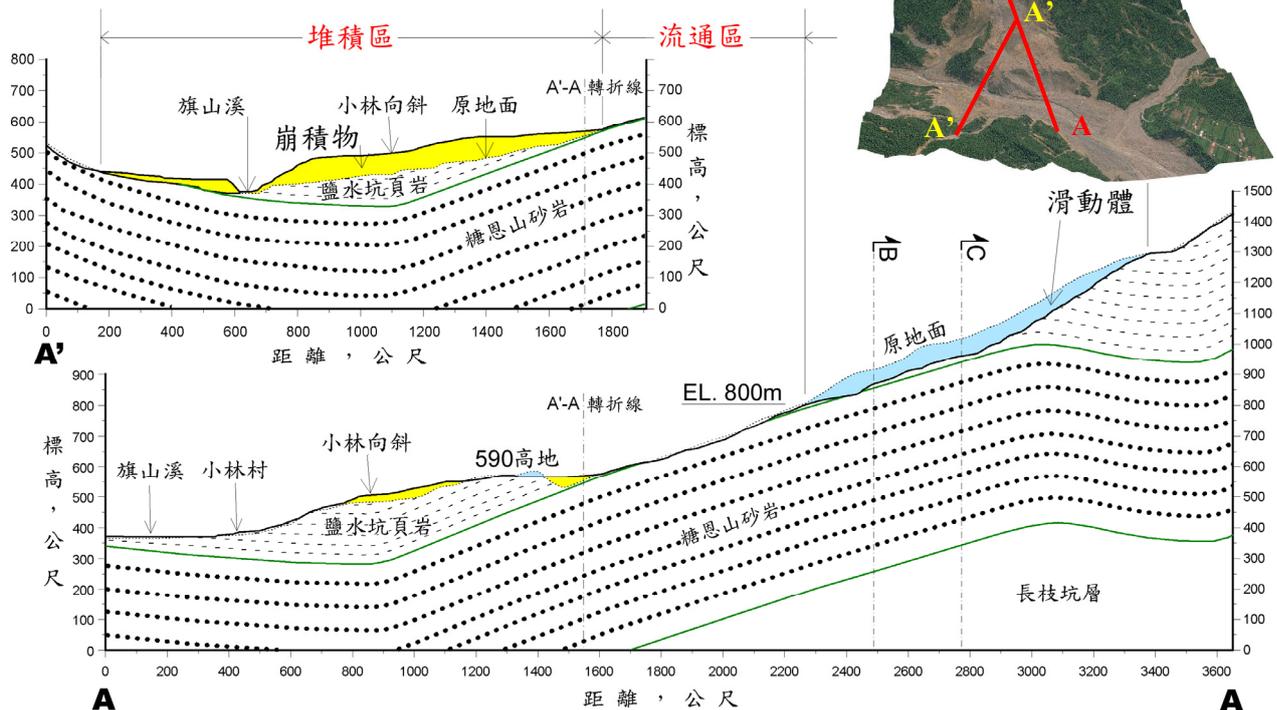


Geology

Introduction- Geologic map (Lee et al., 2010)

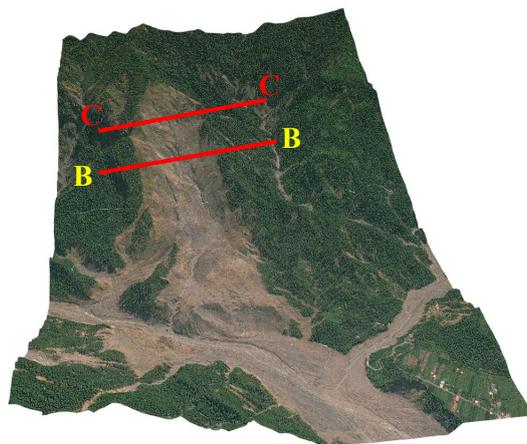
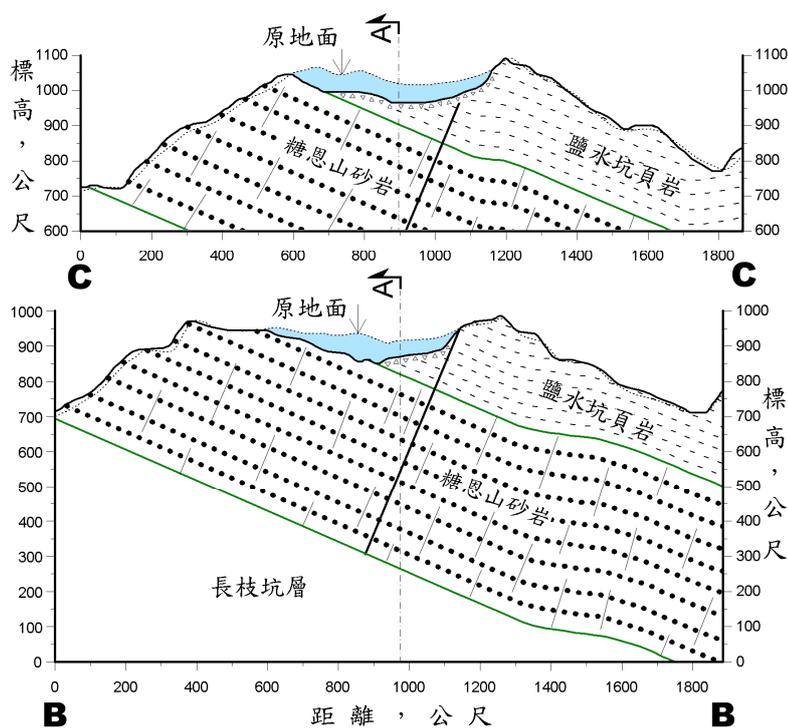


環境地質條件-地質



小林村地質剖面圖A-A，A'-A'切在無名溪A附近，堆積厚度厚

環境地質條件-地質剖面

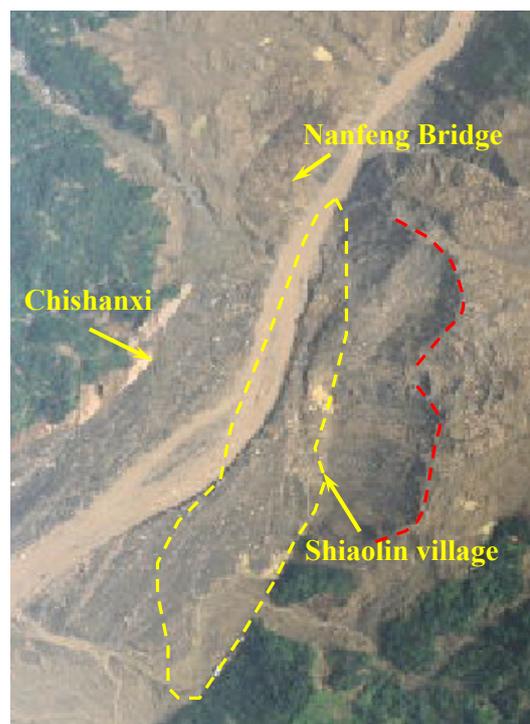


小林村地質剖面圖B-B & C-C

Introduction



Before Morakot Typhoon (2003)



After Morakot Typhoon (2009)

Field investigate

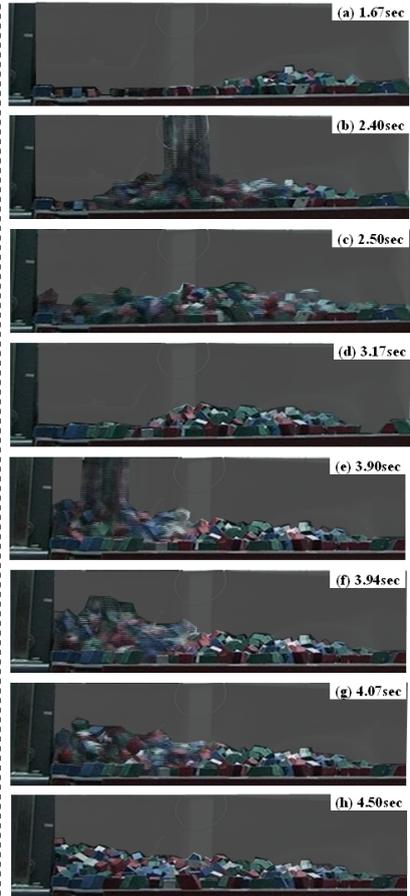
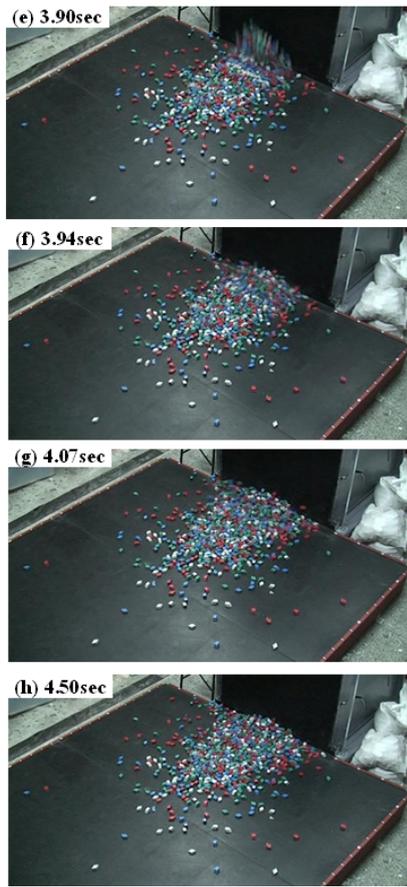
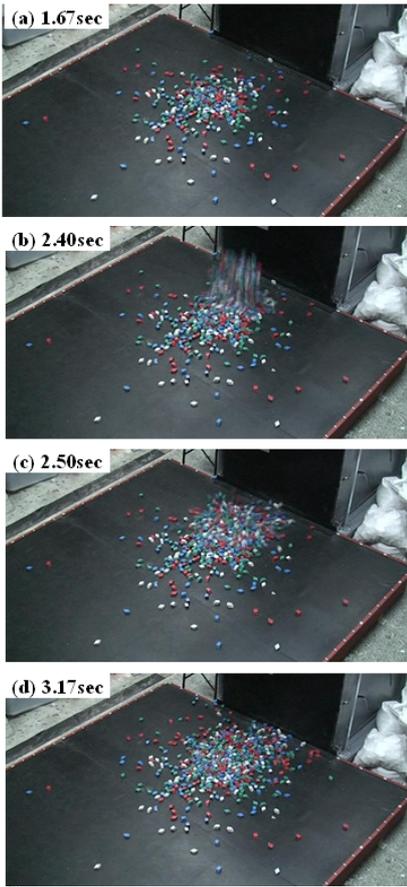






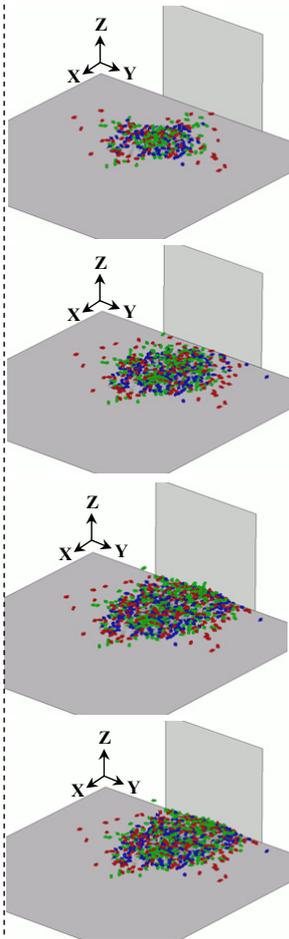
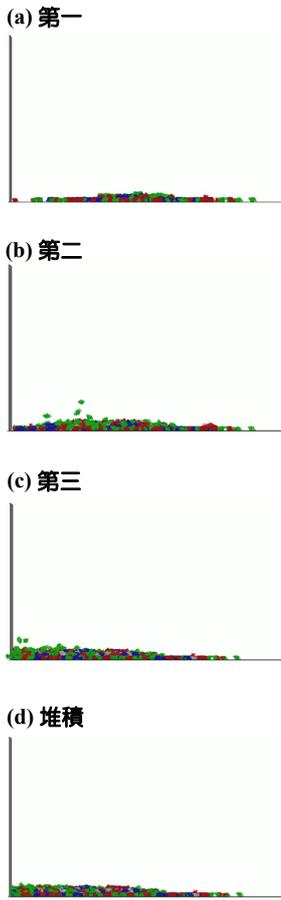


Experiment



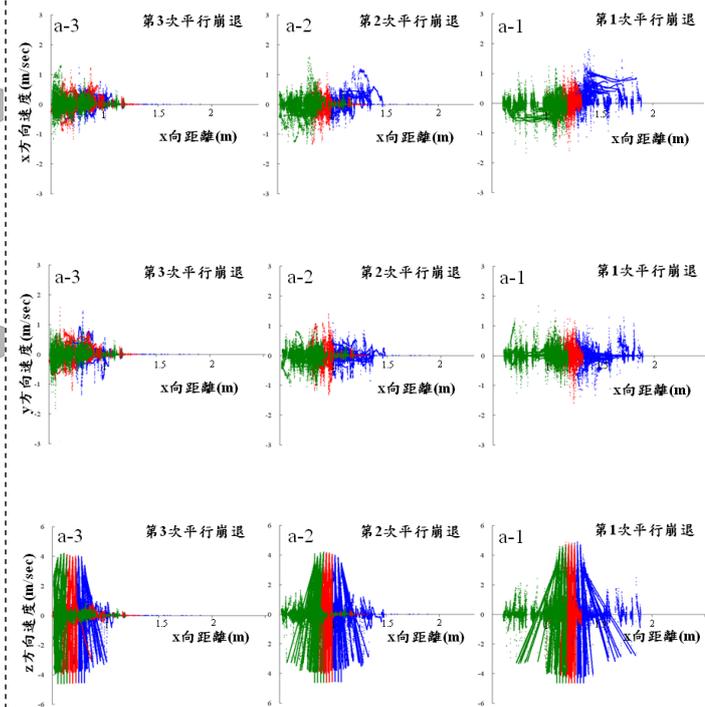
49

側



90度 地 3

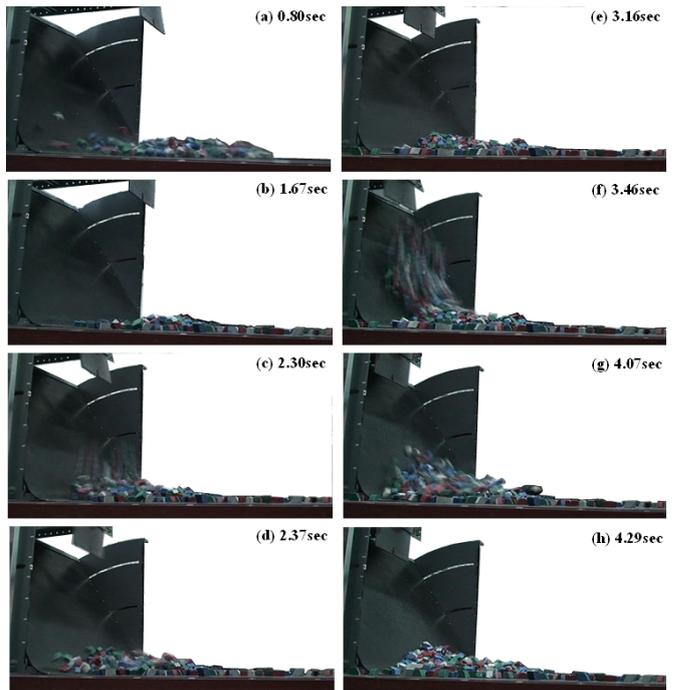
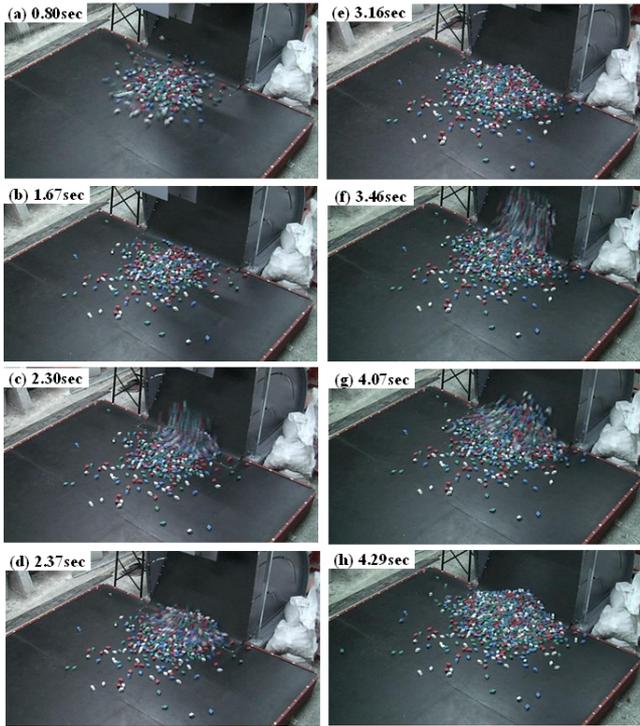
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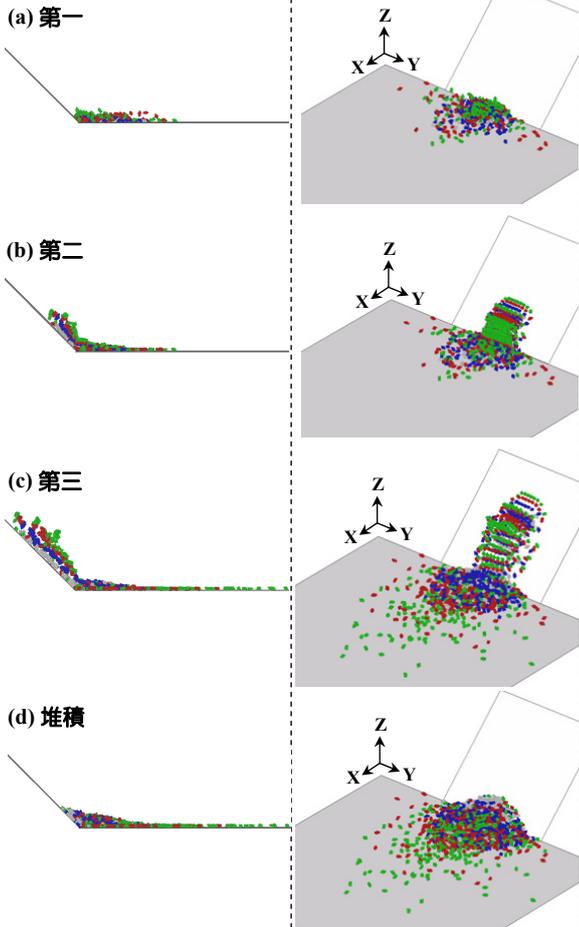
45度 地 3

(360)

堆積

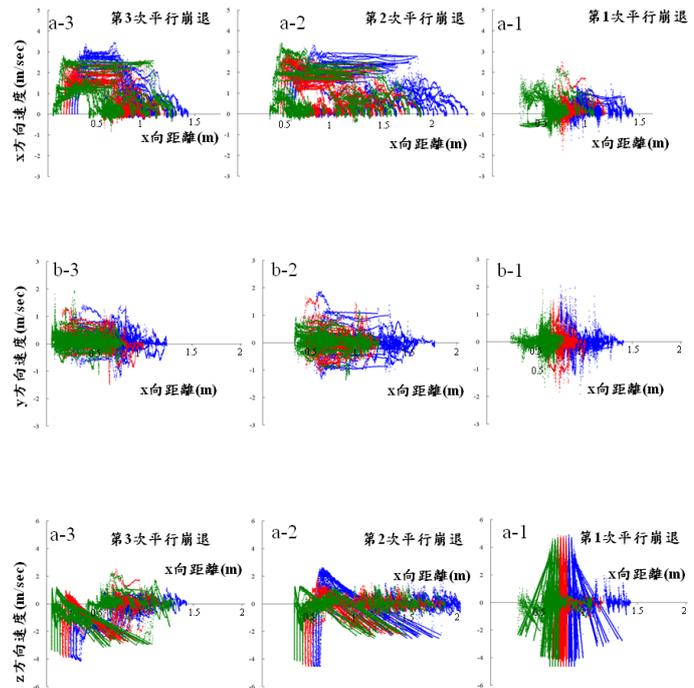


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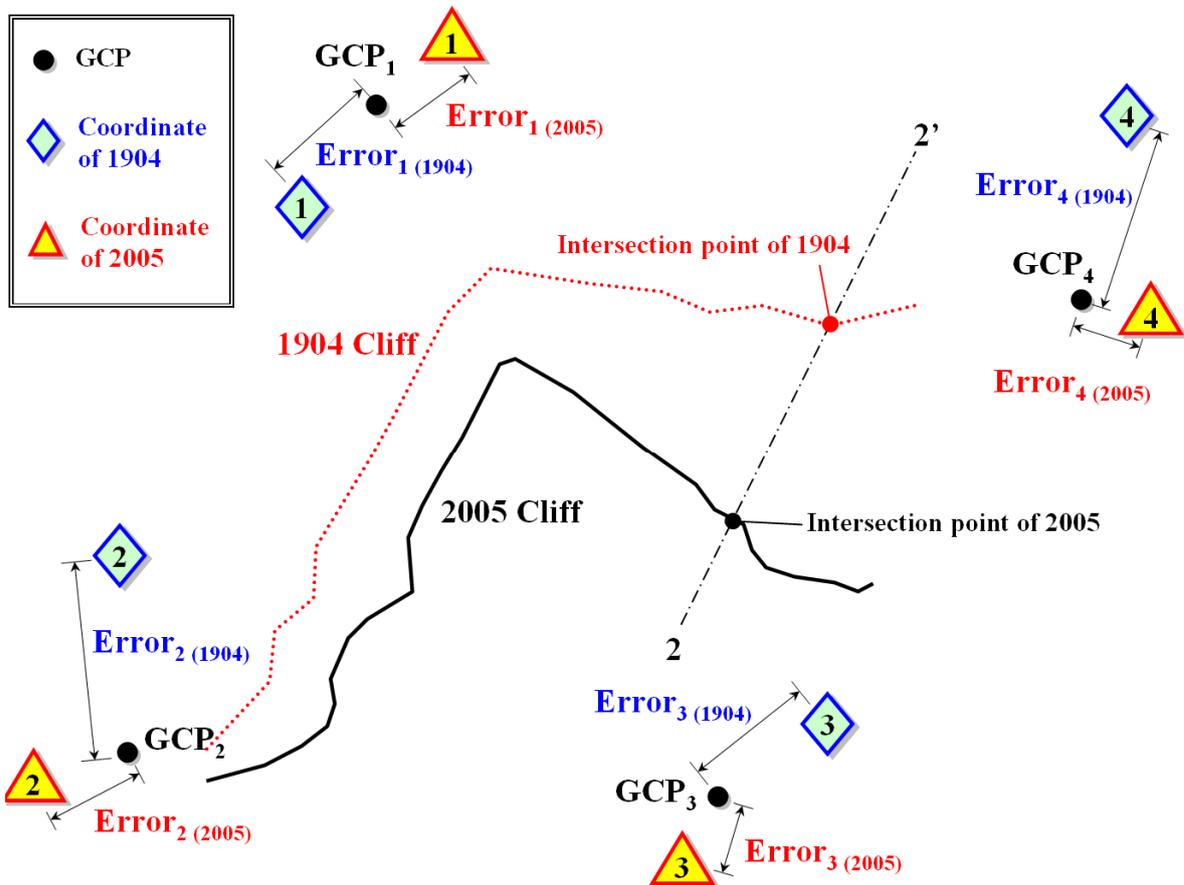
45度 地 3

度 圖



Geomorphologic analysis

(a)



(b)

